

# *William Dale Consulting Engineering*



Project:	47a Market Jew Street
Client:	Mr T Hudson
Author:	Mr Billy Dale
Reference:	2466 – 47a Market Jew St – Calculations
Date:	11 <sup>th</sup> December 2023

*William Dale Consulting Engineering*

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# WDcEng

Job No.	2466	Sheet No.	1	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance  
Member. Proposed room in the extension

<b>Client:</b>	Mr T Hudson
<b>Architect:</b>	My Place Design
<b>Local Authority:</b>	Cornwall County Council
<b>Structure Type:</b>	Existing two storey stone masonry commercial property with typically duo-pitched common truss roof and assumed stone footings.
<b>Proposed Works:</b>	Construction of room in the roof extension and associated works.
<b>Extent of Works:</b>	Design and detailing of structural elements for proposed room in the roof extension.
<b>Design Aids:</b>	<b>BS 5268, BS 5628, BS 5950, BS 648, BS 5977</b>
<b>Drawings:</b>	<b>2466-WDCE-STR-MJSP-M2-S-0001</b>
<b>Remarks:</b>	

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# WDcEng

Job No.	2466	Sheet No.	2	Rev.			
Client.	Mr T Hudson						
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Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

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## STANDARD LOADINGS

Location	Unfactored Loads		Factor $\gamma_f$	Factored Loads	
Sloping Roofs (Measured on plan)					
Slates	0.48	kN/m <sup>2</sup>	1.4	0.67	kN/m <sup>2</sup>
Battens and breather membrane	0.04	kN/m <sup>2</sup>	1.4	0.06	kN/m <sup>2</sup>
Rafters	0.08	kN/m <sup>2</sup>	1.4	0.11	kN/m <sup>2</sup>
Insulation	0.05	kN/m <sup>2</sup>	1.4	0.07	kN/m <sup>2</sup>
Plasterboard + skim	0.20	kN/m <sup>2</sup>	1.4	0.28	kN/m <sup>2</sup>
Live load	0.75	kN/m <sup>2</sup> (max)	1.6	1.20	kN/m <sup>2</sup>
Total	1.60	kN/m <sup>2</sup>		2.39	kN/m <sup>2</sup>
Roof Space					
Joists and insulation	0.20	kN/m <sup>2</sup>	1.4	0.28	kN/m <sup>2</sup>
soffit	0.35	kN/m <sup>2</sup>	1.4	0.49	kN/m <sup>2</sup>
Live load	0.25	kN/m <sup>2</sup>	1.6	0.40	kN/m <sup>2</sup>
Total	0.80	kN/m <sup>2</sup>		1.17	kN/m <sup>2</sup>
Timber Floors					
Boards and joists	0.40	kN/m <sup>2</sup>	1.4	0.56	kN/m <sup>2</sup>
soffit	0.25	kN/m <sup>2</sup>	1.4	0.35	kN/m <sup>2</sup>
Live load (Domestic)	1.50	kN/m <sup>2</sup>	1.6	2.40	kN/m <sup>2</sup>
Total	2.15	kN/m <sup>2</sup>		3.31	kN/m <sup>2</sup>
Masonry Walls					
100mm dense block	2.00	kN/m <sup>2</sup>	1.4	2.80	kN/m <sup>2</sup>
Plaster	0.25	kN/m <sup>2</sup>	1.4	0.35	kN/m <sup>2</sup>
Total	2.25	kN/m <sup>2</sup>		3.15	kN/m <sup>2</sup>

# WD Eng

Job No.	2466	Sheet No.	3	Rev.			
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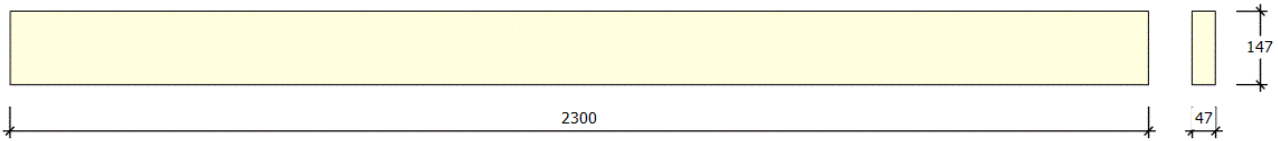
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## MASTERKEY : TIMBER DESIGN

### JOIST DESIGN TO BS 5268 : PART 2

#### Timber Joist



#### Summary Design Data

Section Size	b = 47, h = 147, 147x47 in Strength Class C24
Section Properties (c,cm <sup>4</sup> ,cm <sup>3</sup> )	Area 69.1, Ix 1244.1, Z 169.3
Specification	1 : Internal use in continuously heated building Medium Term loading, Load sharing
Joist data	Span 2.3 m, Spacing 0.4 m, Bearing length B 50, Distance to Bearing 25 mm
Joist loading	Dead load 0.5 kN/m <sup>2</sup> , Live load 1.5 kN/m <sup>2</sup>

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{m,adm} = K_2 \cdot K_3 \cdot K_7 \cdot K_8 \cdot \sigma_m$	1.00 x 1.25 x 1.08 x 1.10 x 7.50	11.15 N/mm <sup>2</sup>
$\sigma_{c,L,adm} = K_2 \cdot K_3 \cdot K_4 \cdot K_8 \cdot \sigma_{c,L}$	1.00 x 1.25 x 1.00 x 1.10 x 1.90	2.61 N/mm <sup>2</sup>
$T_{adm} = K_2 \cdot K_3 \cdot K_8 \cdot T$	1.00 x 1.25 x 1.10 x 0.71	0.98 N/mm <sup>2</sup>
$E = K_2 \cdot E_{mean}$	1.00 x 10800	10800.0 N/mm <sup>2</sup>

#### Design Loads

Density and Selfweight	Timber Density 420 kg/m <sup>3</sup> , Fj 0.03 kN/m	
$w = (F_d + F_l) \cdot s + F_j$	(0.50 + 1.50) x 0.4 + 0.03	0.83 kN/m

#### Bending Check

$M = w \cdot L^2 / 8$	$0.83 \times 2.3^2 / 8$	0.549 kN.m	
$\sigma_{m,a} = M / Z$	$0.549 / 169.27 \leq 11.15$	3.24 N/mm <sup>2</sup>	OK

#### Shear and Bearing Check

$F_v = w \cdot L / 2$	$0.83 \times 2.3 / 2$	0.955 kN	
$T_a = 1.5 F_v / \text{Area}$	$1.5 \times 0.955 / 69.09 \leq 0.98$	0.21 N/mm <sup>2</sup>	OK
$\sigma_{c,L,a} = F_v / (b \cdot B)$	$0.955 / (47 \times 50) \leq 2.61$	0.41 N/mm <sup>2</sup>	OK

#### Deflection Check

$\delta_m = 5 \cdot w \cdot L^4 / (384 \cdot E \cdot I_x)$	$5 \times 0.83 \times 2.3^4 / (384 \times 10800 \times 1244.1)$	2.25 mm	
$\delta_s = 12 \cdot w \cdot L^2 / (5 \cdot E \cdot \text{Area})$	$12 \times 0.83 \times 2.3^2 / (5 \times 10800 \times 69.1)$	0.14 mm	
$\delta = \delta_m + \delta_s$	$2.25 + 0.14 \leq L/333 \text{ or } 14\text{mm}$	2.39 mm	OK

# WDCEng

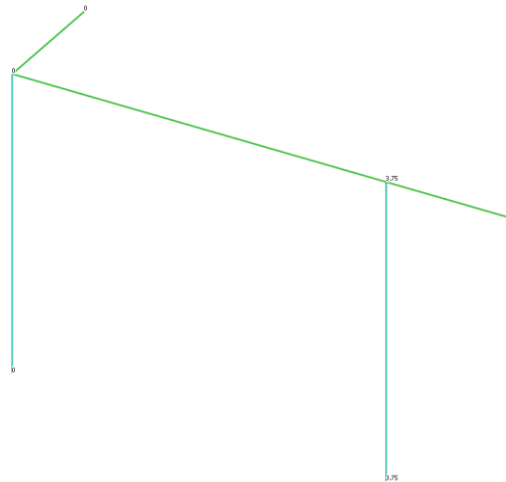
Job No.	2466	Sheet No.	4	Rev.			
Client.	Mr T Hudson						
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Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

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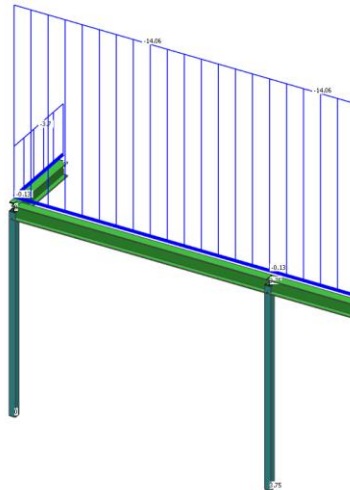
### MasterFrame : Graphics



### Frame Geometry - Full Frame - 3D Front View

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### MasterFrame : Graphics



### Load Diagram - 001 : Dead plus Live (Ultimate) - All Groups Frame Geometry - Full Frame - 3D Front View

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Client.	Mr T Hudson				
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Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Nodal Deflections Serviceability (002 : Live Only (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	-0.05	0.00	0.05	0.00	0.00	0.00	0.00
3-0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4-1	0.00	-0.06	0.00	0.06	0.00	0.00	0.00	0.00
5-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

### Nodal Deflections Serviceability (Maximum Values)

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	-0.05	0.00	0.05	0.00	0.00	0.00	0.00
3-0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4-1	0.00	-0.06	0.00	0.06	0.00	0.00	0.00	0.00
5-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

### Nodal Deflections Serviceability (Minimum Values)

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	-0.05	0.00	0.05	0.00	0.00	0.00	0.00
3-0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4-1	0.00	-0.06	0.00	0.06	0.00	0.00	0.00	0.00
5-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

### Member Forces Ultimate (001 : Dead plus Live (Ultimate))

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	2	0.00C	0.00	26.37	0.00	0.00	0.00	24.72		7.54
	4	0.00C	0.00	-26.37	0.00	0.00	0.00	@ 1.875		@ 1.875
1	4	0.00C	0.00	8.79	0.00	0.00	0.00	2.75		0.09
	5	0.00C	0.00	-8.79	0.00	0.00	0.00	@ 0.625		@ 0.625
0	1	29.08C	0.00	0.00	0.00	0.00	0.00			0.00
	2	28.69C	0.00	0.00	0.00	0.00	0.00			@ 0.000
0	3	35.56C	0.00	0.00	0.00	0.00	0.00			0.00
	4	35.16C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	0.00C	0.00	2.32	0.00	0.00	0.00	0.72		0.02
	6	0.00C	0.00	-2.32	0.00	0.00	0.00	@ 0.613		@ 0.625

### Member Forces Ultimate (Maximum Values)

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	2	0.00C	0.00	26.37	0.00	0.00	0.00	24.72		7.54
	4	0.00C	0.00	-26.37	0.00	0.00	0.00	@ 1.875		@ 1.875
1	4	0.00C	0.00	8.79	0.00	0.00	0.00	2.75		0.09
	5	0.00C	0.00	-8.79	0.00	0.00	0.00	@ 0.625		@ 0.625



# WDcEng

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Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Support Reactions Serviceability (Minimum Values)

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-0	0.000	3.938	0.000	0.000	0.000	0.000
Total	0.000	10.500	0.000	0.000	0.000	0.000



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Member. Proposed room in the extension

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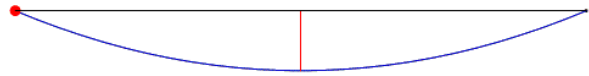
## AXIAL WITH MOMENTS (MEMBER)

### Member SBL1Id 1 @ Level 1 in Load Case 1 : Group Name Here

Member Loading and Member Forces

Loading Combination : 1 UT + 1.4 D1 + 1.6 L1

D1 D 077.010 (kN/m<sup>3</sup>)  
 D1 UDLY -002.400 (kN/m)  
 L1 UDLY -001.100 (kN/m)  
 D1 UDLY -003.200 (kN/m)  
 D1 UDLY -001.400 (kN/m)  
 L1 UDLY -000.700 (kN/m)  
 D1 UDLY -000.400 (kN/m)  
 L1 UDLY -000.300 (kN/m)



#### Member Forces in Load Case 1 and Maximum Deflection from Load Case 2

Member No.	Node End 1 End 2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	2	0.00C	0.00	26.37	0.00	0.00	0.00	24.72		1.13
	4	0.00C	0.00	-26.37	0.00	0.00	0.00	@ 1.875		@ 1.875

### Classification and Properties (BS 5950: 2000)

Section (25.09 kg/m) 203x133 UB 25 [S 275]  
 Class =  $F_n(b/T, d/t, p_y, F, M_x, M_y)$  8.54, 30.25, 275, 0, 24.72, 0 (Axial: Non-Slender) Plastic  
 Auto Design Load Cases 1

### Shear Capacity Check

$F_v/P_v$  26.373 / 191.11 = 0.138 OK

### Moment Capacity Check $M_c$ - Fully Restrained Beam

$F_v/P_v$  0.002 / 191.11 = 0 Low Shear  
 $M_c = p_y.S_{xx} \leq 1.2 p_y.Z_{xx}$  275 x 257.7  $\leq$  1.2 x 275 x 230.42 = 70.868 kN.m  
 $MA/M_c$  24.72 / 70.868 = 0.349 OK

### Deflection Check - Load Case 2

In-span  $\delta \leq \text{Span}/360$  1.13  $\leq$  3750 / 360 1.13 mm OK

# WD Eng

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Member. Proposed room in the extension

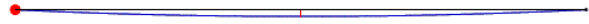
## AXIAL WITH MOMENTS (MEMBER)

### Member SBL1Id 2 @ Level 1 in Load Case 1 : Group Name Here

Member Loading and Member Forces

Loading Combination : 1 UT + 1.4 D1 + 1.6 L1

D1 D 077.010 (kN/m<sup>3</sup>)  
D1 UDLY -002.400 (kN/m)  
L1 UDLY -001.100 (kN/m)  
D1 UDLY -003.200 (kN/m)  
D1 UDLY -001.400 (kN/m)  
L1 UDLY -000.700 (kN/m)  
D1 UDLY -000.400 (kN/m)  
L1 UDLY -000.300 (kN/m)



#### Member Forces in Load Case 1 and Maximum Deflection from Load Case 2

Member No.	Node End 1 End 2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	4	0.00C	0.00	8.79	0.00	0.00	0.00	2.75		0.01
	5	0.00C	0.00	-8.79	0.00	0.00	0.00	@ 0.625		@ 0.625

### Classification and Properties (BS 5950: 2000)

Section (25.09 kg/m) 203x133 UB 25 [S 275]  
Class = Fn(b/T,d/t,py,F,Mx,My) 8.54, 30.25, 275, 0, 2.75, 0 (Axial: Non-Slender) Plastic  
Auto Design Load Cases 1

### Shear Capacity Check

Fvx/Pvx 8.79 / 191.11 = 0.046 OK

### Moment Capacity Check Mc - Fully Restrained Beam

Fv/Pv 0.002 / 191.11 = 0 Low Shear  
Mc = py.Sxx ≤ 1.2 py.Zxx 275 x 257.7 ≤ 1.2 x 275 x 230.42 = 70.868 kN.m  
MA/Mc 2.745 / 70.868 = 0.039 OK

### Deflection Check - Load Case 2

In-span δ ≤ Span/360 0.01 ≤ 1250 / 360 0.01 mm OK

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## AXIAL WITH MOMENTS (MEMBER)

### Member SCL1Id 3 @ Level 1 in Load Case 1 : Design group 2

Member Loading and Member Forces

Loading Combination : 1 UT + 1.4 D1 + 1.6 L1

D1 D 077.010 (kN/m<sup>3</sup>)



#### Member Forces in Load Case 1

Member No.	Node End 1 End 2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
0	1	29.08C	0.00	0.00	0.00	0.00	0.00			0.00
	2	28.69C	0.00	0.00	0.00	0.00	0.00			@ 0.625

#### Additional Nominal Moments

MxUp, MyUp 3.824 kN.m, -0.336 kN.m

#### Classification and Properties (BS 5950: 2000)

Section (9.66 kg/m) 90x90x3.6 SHS 9.66 [S 275]

Class = Fn(b/t,d/t,py,F,Mx,My) 22, 22, 275, 29.084, 3.824, 0.336

(Axial: Non-Slender)

Plastic

Auto Design Load Cases

1

#### Local Capacity Check

Fvx/Pvx	0 / 101.475 =	0	Low Shear
Mcx = py.Sxx ≤ 1.2 py.Zxx	275 x 39.69 ≤ 1.2 x 275 x 33.8 =	10.915 kN.m	
Fvy/Pvy	0 / 101.475 =	0	Low Shear
Mcy = py.Syy ≤ 1.2 py.Zyy	275 x 39.69 ≤ 1.2 x 275 x 33.8 =	10.915 kN.m	
Pz = Ag.py	12.3 x 275 =	338.25 kN	
n = F/Pz	29.084 / 338.25 =	0.086	OK
Srx = Fn(Sxx,)	39.69, 0.086	39.3 cm <sup>3</sup>	
Mrx = Srx.py	39.3 x 275	10.808 kN.m	
Sry = Fn(Syy,)	39.69, 0.086	39.3 cm <sup>3</sup>	
Mry = Sry.py	39.3 x 275	10.808 kN.m	
(Mx/Mrx) <sup>2.1</sup> + (My/Mry) <sup>2.2</sup>	(3.824/10.808) <sup>1.667</sup> + (0.336/10.808) <sup>1.667</sup> =	0.18	OK

#### Compression Resistance Pc

λx = Lex/rxx	100x1x3/3.52 =	85.2	OK
Pcx = Area.pcx	12.3x191.53/10 =	235.581 kN	Table 24 a
λy = Ley/ryy	100x1x3/3.52 =	85.2	OK
Pcy = Area.pcy	12.3x191.53/10 =	235.581 kN	Table 24 a

#### Equivalent Uniform Moment Factors mLT, mx, my and myx

mLT = 0.2 + (.15M2 + .5M3 + .15M4) / Mmax	0.2 + (.15x1 + .5x2 + .15x3) / 4 = 0.44	0.6	Table 18
my = 0.2 + (.1M2 + .6M3 + .1M4) / Mmax	0.2 + (.1x0 + .6x0 + .1x0) / 0 = .8x0/0	0.6	Table 26
mx = 0.2 + (.1M2 + .6M3 + .1M4) / Mmax	0.2 + (.1x1 + .6x2 + .1x3) / 4 = .8x3/4	0.6	Table 26
myx = 0.2 + (.1M2 + .6M3 + .1M4) / Mmax	0.2 + (.1x0 + .6x0 + .1x0) / 0 = .8x0/0	0.6	Table 26

#### Lateral Buckling Check Mb

Mb = Mc Section not susceptible to lateral torsional buckling 10.915 kN.m

# WDcEng

Job No.	2466	Sheet No.	11	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

## Combined Axial Compression and Bending to Annex I

$r_b = m_{LT} \cdot M_{LT} / M_b$	0.6x3.8/10.9	0.210	
$r_c = F_c / P_{cY}$	29.1/235.6	0.123	
$\lambda_r = (r_b \lambda_{LT} + r_c \lambda_y) / (r_b + r_c)$	(0.21*0+0.123*85.2)/(0.21+0.123)	31.531	
$\lambda_o = 17.15 \varepsilon (2r_b + r_c) / (r_b + r_c)$	17.15*1(2*0.21+0.123)/(0.21+0.123)	27.955	
$M_{ob} = M_b(1 - F_c / P_{cY})$	10.915(1 - 29.1/235.6)	9.567	
$M_{xy} = 2M_{cX} (1 - F_c / P_{cY})$	2*10.915(1 - 29.1/235.6)	19.134	
$M_{ox} = M_{cX}(1 - F_c / P_{cX}) / (1 + 0.5F_c / P_{cX})$	10.915(1 - 29.1/235.6) / (1 + 0.5*29.1/235.6)	9.011	
$M_{oy} = M_{cY}(1 - F_c / P_{cY}) / (1 + k_y(F_c / P_{cY}))$	10.915(1 - 29.1/235.6) / (1 + 0.5(29.1/235.6))	9.011	
$M_{ab} = \text{fn}(\lambda_r, \lambda_o, \varepsilon, M_{xy}, M_{ob})$	31.531, 27.955, 1.000, 19.134, 9.567	10.731	
$M_{ax} = \text{fn}(\lambda_x, \varepsilon, M_{rx}, M_{ox})$	85.227, 1.000, 10.808, 9.011	9.026	
$M_{ay} = \text{fn}(\lambda_y, \varepsilon, M_{ry}, M_{oy})$	85.227, 1.000, 10.808, 9.011	9.026	
$m_x \cdot M_x / M_{ax} + .5m_y \cdot M_y / M_{cY}(1 - F_c / P_{cX})$	0.6x3.8/9 + .5x0.6x0.3/(10.9(1 - 29.1/235.6))	0.265	OK
$m_{LT} \cdot M_{LT} / M_{ab} + m_y \cdot M_y / M_{ay}$	0.6x3.8/10.7 + 0.6x-0.3/9	0.236	OK
$m_x \cdot M_x / M_{ax} + m_y \cdot M_y / M_{ay}$	0.6x3.8/9 + 0.6x-0.3/9	0.277	OK
Compare with Simplified to 4.8.3.3	0.392, 0.355, 0.355	0.392	
Compare with MoreExact to 4.8.3.3	0.356, 0.248, 0.277	0.356	

Job No.	2466	Sheet No.	12	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

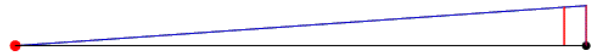
## AXIAL WITH MOMENTS (MEMBER)

### Member SCL1Id 4 @ Level 1 in Load Case 1 : Design group 2

Member Loading and Member Forces

Loading Combination : 1 UT + 1.4 D1 + 1.6 L1

D1 D 077.010 (kN/m<sup>3</sup>)



#### Member Forces in Load Case 1

Member No.	Node End 1 End 2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
0	3	35.56C	0.00	0.00	0.00	0.00	0.00			0.00
	4	35.16C	0.00	0.00	0.00	0.00	0.00			@ 0.625

#### Additional Nominal Moments

MxUp -2.549 kN.m

#### Classification and Properties (BS 5950: 2000)

Section (9.66 kg/m)

Class = Fn(b/t,d/t,py,F,Mx,My) 22, 22, 275, 35.559, 2.549, 0

(Axial: Non-Slender)

Plastic

Auto Design Load Cases

1

#### Local Capacity Check

Fvx/Pvx	0 / 101.475 =	0	Low Shear
Mcx = py.Sxx ≤ 1.2 py.Zxx	275 x 39.69 ≤ 1.2 x 275 x 33.8 =	10.915 kN.m	
Pz = Ag.py	12.3 x 275 =	338.25 kN	
n = F/Pz	35.559 / 338.25 =	0.105	OK
Srx = Fn(Sxx,)	39.69, 0.105	39.11 cm <sup>3</sup>	
Mrx = Srx.py	39.11 x 275	10.755 kN.m	
(Mx/Mrx) <sup>2.1</sup> + (My/Mry) <sup>2.2</sup>	(2.549/10.755) <sup>1.667</sup> + (0) <sup>1.667</sup> =	0.091	OK

#### Compression Resistance Pc

λx = Lex/rxx	100x1x3/3.52 =	85.2	OK
Pcx = Area.pcx	12.3x191.53/10 =	235.581 kN	Table 24 a
λy = Ley/ryy	100x1x3/3.52 =	85.2	OK
Pcy = Area.pcy	12.3x191.53/10 =	235.581 kN	Table 24 a

#### Equivalent Uniform Moment Factors mLT, mx, my and myx

mLT = 0.2 + (.15M2 + .5M3 + .15M4)/Mmax	0.2 + (.15x1 + .5x1 + .15x2)/3 = 0.44	0.6	Table 18
my = 0.2 + (.1M2 + .6M3 + .1M4)/Mmax	0.2 + (.1x0 + .6x0 + .1x0)/0 = .8x0/0	1	Table 26
mx = 0.2 + (.1M2 + .6M3 + .1M4)/Mmax	0.2 + (.1x-1 + .6x-1 + .1x-2)/3 = .8x2/3	0.6	Table 26
myx = 0.2 + (.1M2 + .6M3 + .1M4)/Mmax	0.2 + (.1x0 + .6x0 + .1x0)/0 = .8x0/0	1	Table 26

#### Lateral Buckling Check Mb

Mb = Mc Section not susceptible to lateral torsional buckling 10.915 kN.m

#### Combined Axial Compression and Bending to Annex I

rb = mLT.MLT/Mb	0.6x-2.5/10.9	0.135
rc = Fc/Pcy	35.6/235.6	0.151
λr = (rb λLT + rc λy)/(rb + rc)	(0.135*0 + 0.151*85.2)/(0.135 + 0.151)	45.029
λro = 17.15 ε (2rb + rc)/(rb + rc)	17.15*1(2*0.135 + 0.151)/(0.135 + 0.151)	25.239

# WDCEng

Job No.	2466	Sheet No.	13	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

**Job Title.** 47a Market Jew Street, Penzance

**Member.** Proposed room in the extension

$M_{ob} = M_b(1-F_c/P_{cy})$	10.915(1-35.6/235.6)	9.267	
$M_{xy} = 2M_{cx}(1-F_c/P_{cy})$	2•10.915(1-35.6/235.6)	18.535	
$M_{ox} = M_{cx}(1-F_c/P_{cx})/(1+0.5F_c/P_{cx})$	10.915(1-35.6/235.6)/(1+0.5•35.6/235.6)	8.617	
$M_{oy} = M_{cy}(1-F_c/P_{cy})/(1+k_y(F_c/P_{cy}))$	10.915(1-35.6/235.6)/(1+0.5(35.6/235.6))	8.617	
$M_{ab} = \text{fn}(\lambda_r, \lambda_{r0}, \epsilon, M_{xy}, M_{ob})$	45.029, 25.239, 1.000, 18.535, 9.267	10.269	
$M_{ax} = \text{fn}(\lambda_x, \epsilon, M_{rx}, M_{ox})$	85.227, 1.000, 10.755, 8.617	8.635	
$M_{ay} = \text{fn}(\lambda_y, \epsilon, M_{ry}, M_{oy})$	85.227, 1.000, 10.755, 8.617	8.635	
$m_{x \cdot M_x/M_{ax}}$	0.6x2.5/8.6	0.177	OK
$m_{LT \cdot M_{LT}/M_{ab}}$	0.6x-2.5/10.3	0.143	OK
$m_{x \cdot M_x/M_{ax}}$	0.6x2.5/8.6	0.170	OK
Compare with Simplified to 4.8.3.3	0.316, 0.286, 0.286	0.316	
Compare with MoreExact to 4.8.3.3	0.302, 0.218, 0.171	0.302	

# WDceng

Job No.	2466	Sheet No.	14	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

## AXIAL WITH MOMENTS (MEMBER)

### Member SBL1Id 5 @ Level 1 in Load Case 1 : Group Name Here

Member Loading and Member Forces  
Loading Combination : 1 UT + 1.4 D1 + 1.6 L1

D1 D 077.010 (kN/m<sup>3</sup>)  
D1 UDLY -002.400 (kN/m)

#### Member Forces in Load Case 1

Member No.	Node End 1 End 2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	2	0.00C	0.00	2.32	0.00	0.00	0.00	0.72		0.00
	6	0.00C	0.00	-2.32	0.00	0.00	0.00	@ 0.613		@ 0.625

### Classification and Properties (BS 5950: 2000)

Section (25.09 kg/m) 203x133 UB 25 [S 275]  
Class = Fn(b/T,d/t,py,F,Mx,My) 8.54, 30.25, 275, 0, 0.72, 0 (Axial: Non-Slender) Plastic  
Auto Design Load Cases 1

### Shear Capacity Check

Fvx/Pvx 2.315 / 191.11 = 0.012 OK

### Moment Capacity Check Mc - Fully Restrained Beam

Fv/Pv 0.001 / 191.11 = 0 Low Shear  
Mc = py.Sxx ≤ 1.2 py.Zxx 275 x 257.7 ≤ 1.2 x 275 x 230.42 = 70.868 kN.m  
MA/Mc 0.721 / 70.868 = 0.010 OK





# W D Ceng

Job No.	2466	Sheet No.	16	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Nodal Deflections Serviceability (002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.06	0.01	0.06	0.03	0.03	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.37	0.00	-0.28	0.47
8-1	0.00	0.00	0.00	0.00	-0.09	0.00	0.07	0.12
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.40	0.00	-0.24	0.47
11-1	0.00	0.00	0.00	0.00	-0.21	0.00	-0.05	0.22

### Nodal Deflections Serviceability (007 : Live Only 1.00L1 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.00	-0.01	0.00	0.01	0.01	0.01	0.01	0.02
6-1	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.01
7-1	0.00	0.00	0.00	0.00	0.13	0.00	-0.10	0.16
8-1	0.00	0.00	0.00	0.00	-0.03	0.00	0.02	0.04
9-1	0.00	0.00	0.00	0.00	-0.02	0.00	-0.01	0.02
10-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.08	0.16
11-1	0.00	0.00	0.00	0.00	-0.07	0.00	-0.02	0.07

### Nodal Deflections Serviceability (008 : Dead Only 1.00D0+1.00D1 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

### Nodal Deflections Serviceability (010 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W1 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.06	0.03	0.02	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.34	0.00	-0.26	0.43
8-1	0.00	0.00	0.00	0.00	-0.08	0.00	0.07	0.11
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.37	0.00	-0.23	0.44
11-1	0.00	0.00	0.00	0.00	-0.20	0.00	-0.05	0.20

# WD CEng

Job No.	2466	Sheet No.	17	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Nodal Deflections Serviceability (012 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W2 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.06	0.03	0.02	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.34	0.00	-0.26	0.43
8-1	0.00	0.00	0.00	0.00	-0.08	0.00	0.07	0.11
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.37	0.00	-0.23	0.44
11-1	0.00	0.00	0.00	0.00	-0.20	0.00	-0.05	0.20

### Nodal Deflections Serviceability (014 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W3 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.06	0.03	0.02	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.34	0.00	-0.26	0.43
8-1	0.00	0.00	0.00	0.00	-0.08	0.00	0.07	0.11
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.37	0.00	-0.23	0.44
11-1	0.00	0.00	0.00	0.00	-0.20	0.00	-0.05	0.20

### Nodal Deflections Serviceability (016 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W4 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.06	0.03	0.02	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.34	0.00	-0.26	0.43
8-1	0.00	0.00	0.00	0.00	-0.08	0.00	0.07	0.11
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.37	0.00	-0.23	0.44
11-1	0.00	0.00	0.00	0.00	-0.20	0.00	-0.05	0.20

### Nodal Deflections Serviceability (018 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W5 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.06	0.03	0.02	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.34	0.00	-0.26	0.43
8-1	0.00	0.00	0.00	0.00	-0.08	0.00	0.07	0.11
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.37	0.00	-0.23	0.44
11-1	0.00	0.00	0.00	0.00	-0.20	0.00	-0.05	0.20

# WD CEng

Job No.	2466	Sheet No.	18	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Nodal Deflections Serviceability (020 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W6 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.06	0.03	0.02	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.34	0.00	-0.26	0.43
8-1	0.00	0.00	0.00	0.00	-0.08	0.00	0.07	0.11
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.37	0.00	-0.23	0.44
11-1	0.00	0.00	0.00	0.00	-0.20	0.00	-0.05	0.20

### Nodal Deflections Serviceability (022 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W7 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.06	0.03	0.02	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.34	0.00	-0.26	0.43
8-1	0.00	0.00	0.00	0.00	-0.08	0.00	0.07	0.11
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.37	0.00	-0.23	0.44
11-1	0.00	0.00	0.00	0.00	-0.20	0.00	-0.05	0.20

### Nodal Deflections Serviceability (024 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W8 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.06	0.03	0.02	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.34	0.00	-0.26	0.43
8-1	0.00	0.00	0.00	0.00	-0.08	0.00	0.07	0.11
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.37	0.00	-0.23	0.44
11-1	0.00	0.00	0.00	0.00	-0.20	0.00	-0.05	0.20

### Nodal Deflections Serviceability (026 : Dead+Wind 1.00D0+1.00D1+1.00W1 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

# WD Eng

Job No.	2466	Sheet No.	19	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Nodal Deflections Serviceability (028 : Dead+Wind 1.00D0+1.00D1+1.00W2 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

### Nodal Deflections Serviceability (030 : Dead+Wind 1.00D0+1.00D1+1.00W3 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

### Nodal Deflections Serviceability (032 : Dead+Wind 1.00D0+1.00D1+1.00W4 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

### Nodal Deflections Serviceability (034 : Dead+Wind 1.00D0+1.00D1+1.00W5 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

# WD CEng

Job No.	2466	Sheet No.	20	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Nodal Deflections Serviceability (036 : Dead+Wind 1.00D0+1.00D1+1.00W6 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

### Nodal Deflections Serviceability (038 : Dead+Wind 1.00D0+1.00D1+1.00W7 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

### Nodal Deflections Serviceability (040 : Dead+Wind 1.00D0+1.00D1+1.00W8 (Serviceability))

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.05	0.01	0.05	0.02	0.02	0.02	0.04
6-1	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.03
7-1	0.00	0.00	0.00	0.00	0.24	0.00	-0.19	0.31
8-1	0.00	0.00	0.00	0.00	-0.06	0.00	0.05	0.08
9-1	0.00	0.00	0.00	0.00	-0.05	0.00	-0.03	0.05
10-1	0.00	0.00	0.00	0.00	-0.26	0.00	-0.16	0.31
11-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.03	0.15

### Nodal Deflections Serviceability (Maximum Values)

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
3-1	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01	0.01
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.02	-0.06	0.01	0.06	0.03	0.03	0.03	0.05
6-1	0.00	0.00	0.00	0.00	0.04	0.00	0.02	0.04
7-1	0.00	0.00	0.00	0.00	0.37	0.00	-0.28	0.47
8-1	0.00	0.00	0.00	0.00	-0.09	0.00	0.07	0.12
9-1	0.00	0.00	0.00	0.00	-0.06	0.00	-0.04	0.07
10-1	0.00	0.00	0.00	0.00	-0.40	0.00	-0.24	0.47
11-1	0.00	0.00	0.00	0.00	-0.21	0.00	-0.05	0.22

# WD Eng

Job No.	2466	Sheet No.	21	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Nodal Deflections Serviceability (Minimum Values)

Load Case	Nodal Displacements (mm)				Nodal Rotation (degrees)			
	$\delta X \rightarrow$	$\delta Y \uparrow$	$\delta Z \nearrow$	$\delta XYZ$	$\theta X \rightarrow$	$\theta Y \uparrow$	$\theta Z \nearrow$	$\theta XYZ$
1-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5-1	0.00	-0.01	0.00	0.01	0.01	0.01	0.01	0.02
6-1	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.01
7-1	0.00	0.00	0.00	0.00	0.13	0.00	-0.10	0.16
8-1	0.00	0.00	0.00	0.00	-0.03	0.00	0.02	0.04
9-1	0.00	0.00	0.00	0.00	-0.02	0.00	-0.01	0.02
10-1	0.00	0.00	0.00	0.00	-0.14	0.00	-0.08	0.16
11-1	0.00	0.00	0.00	0.00	-0.07	0.00	-0.02	0.07

### Member Forces Ultimate (001 : Dead+Live 1.40D0+1.40D1+1.60L1 (Ultimate))

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.39	0.00	0.00	0.00	0.28		0.00
	2	0.00C	0.00	-1.39	0.00	0.00	0.00	@ 0.384		@ 0.000
1	2	0.00C	0.00	0.81	0.00	0.00	0.00	0.09		0.00
	3	0.00C	0.00	-0.84	0.00	0.00	0.00	@ 0.223		@ 0.000
1	3	0.00C	0.00	4.26	0.00	0.00	0.00	2.71		0.05
	8	0.00C	0.00	-2.13	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	2.14T	0.00	3.20	0.00	-0.51	0.00	0.22	0.00	0.10
	5	2.14T	0.00	-1.35	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.82C	-0.01	0.11	0.01	0.00	-0.01	0.03		0.35
	5	2.24C	0.01	-0.56	0.01	-0.75	0.02	@ 0.536		@ 2.279
1	3	0.32C	-0.01	0.13	0.01	0.00	-0.01	0.04		0.55
	6	0.32T	0.01	-0.62	0.01	-0.91	0.04	@ 0.600		@ 2.512
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.80T	0.02	-0.56	0.95	-0.09	-0.14			0.06
	6	2.80T	-0.02	-2.61	0.95	-1.07	0.43			@ 0.371
1	5	1.61C	0.01	-1.65	0.05	0.77	-0.13	-1.05		1.79
	9	2.82C	-0.01	1.49	0.05	-0.03	0.04	@ 2.054		@ 1.845
1	6	1.62T	-0.14	3.92	-0.76	-2.66	0.70	0.72	-1.33	2.29
	7	1.25C	0.14	-1.23	-0.76	0.20	-1.33	@ 1.843	@ 2.668	@ 1.788
1	7	0.64T	0.21	1.61	-0.72	-1.18	1.31			
	8	0.36C	-0.21	-0.18	-0.72	0.00	-0.37			
1	6	0.68T	0.00	-1.65	-0.01	0.79	0.01	-1.15		1.89
	9	0.86C	0.00	1.53	-0.01	0.03	-0.02	@ 1.950		@ 1.840
1	6	0.00C	0.00	-5.37	0.00	2.94	0.00	-2.06		4.38
	11	0.00C	0.00	3.67	0.00	0.00	0.00	@ 1.806		@ 1.687

# WD Eng

Job No.	2466	Sheet No.	22	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (001 : Dead+Live 1.40D0+1.40D1+1.60L1 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.44T	0.00	14.56	0.03	-2.10	-0.06	14.37		13.80
	10	0.44C	0.00	-13.60	0.03	0.00	0.06	@ 2.275		@ 2.231

**Member Forces Ultimate (003 : Dead+Live 1.40D0+1.40D1+1.60L1+EHL@0)**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.39	0.00	0.00	0.00	0.28		0.00
	2	0.00C	0.00	-1.39	0.00	0.00	0.00	@ 0.384		@ 0.000
1	2	0.00C	0.00	0.81	0.00	0.00	0.00	0.09		0.00
	3	0.00C	0.00	-0.84	0.00	0.00	0.00	@ 0.223		@ 0.000
1	3	0.00C	0.00	4.26	0.00	0.00	0.00	2.71		0.05
	8	0.00C	0.00	-2.13	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	2.15T	0.00	3.20	0.00	-0.51	0.00	0.22	0.00	0.10
	5	2.15T	0.00	-1.35	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.82C	-0.01	0.11	0.01	0.00	-0.01	0.03		0.35
	5	2.25C	0.01	-0.56	0.01	-0.75	0.02	@ 0.536		@ 2.279
1	3	0.32C	-0.01	0.13	0.01	0.00	-0.01	0.04		0.55
	6	0.32T	0.01	-0.62	0.01	-0.91	0.04	@ 0.600		@ 2.512
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.79T	0.02	-0.56	0.95	-0.09	-0.14			0.06
	6	2.78T	-0.02	-2.61	0.95	-1.07	0.43			@ 0.371
1	5	1.61C	0.01	-1.65	0.05	0.77	-0.13	-1.05		1.79
	9	2.82C	-0.01	1.49	0.05	-0.03	0.04	@ 2.054		@ 1.845
1	6	1.62T	-0.14	3.92	-0.76	-2.66	0.70	0.72	-1.33	2.29
	7	1.25C	0.14	-1.23	-0.76	0.20	-1.33	@ 1.843	@ 2.668	@ 1.788
1	7	0.64T	0.21	1.61	-0.72	-1.18	1.31			
	8	0.36C	-0.21	-0.18	-0.72	0.00	-0.37			
1	6	0.68T	0.00	-1.65	-0.01	0.79	0.01	-1.15		1.89
	9	0.86C	0.00	1.53	-0.01	0.03	-0.02	@ 1.950		@ 1.840
1	6	0.00C	0.00	-5.37	0.00	2.94	0.00	-2.06		4.38
	11	0.00C	0.00	3.67	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000

# WD Eng

Job No.	2466	Sheet No.	23	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (003 : Dead+Live 1.40D0+1.40D1+1.60L1+EHL@0)**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	7	0.44T	0.00	14.56	0.03	-2.10	-0.06	14.37		13.80
	10	0.44C	0.00	-13.60	0.03	0.00	0.06	@ 2.275		@ 2.231

**Member Forces Ultimate (004 : Dead+Live 1.40D0+1.40D1+1.60L1+EHL@90)**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.39	0.00	0.00	0.00	0.28		0.00
	2	0.00C	0.00	-1.39	0.00	0.00	0.00	@ 0.384		@ 0.000
1	2	0.00C	0.00	0.81	0.00	0.00	0.00	0.09		0.00
	3	0.00C	0.00	-0.84	0.00	0.00	0.00	@ 0.223		@ 0.000
1	3	0.00C	0.00	4.26	0.00	0.00	0.00	2.71		0.05
	8	0.00C	0.00	-2.13	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	2.14T	0.00	3.20	0.00	-0.51	0.00	0.22	0.00	0.10
	5	2.14T	0.00	-1.35	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.81C	-0.01	0.11	0.01	0.00	-0.01	0.03		0.35
	5	2.24C	0.01	-0.56	0.01	-0.75	0.02	@ 0.536		@ 2.279
1	3	0.32C	-0.01	0.13	0.01	0.00	-0.01	0.04		0.55
	6	0.32T	0.01	-0.62	0.01	-0.91	0.04	@ 0.600		@ 2.512
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.80T	0.02	-0.56	0.95	-0.09	-0.14			0.06
	6	2.79T	-0.02	-2.61	0.95	-1.07	0.43			@ 0.371
1	5	1.63C	0.01	-1.65	0.05	0.77	-0.13	-1.05		1.79
	9	2.84C	-0.01	1.49	0.05	-0.03	0.04	@ 2.054		@ 1.845
1	6	1.62T	-0.14	3.92	-0.76	-2.66	0.70	0.72	-1.33	2.29
	7	1.25C	0.14	-1.23	-0.76	0.20	-1.33	@ 1.843	@ 2.668	@ 1.788
1	7	0.64T	0.21	1.61	-0.72	-1.18	1.31			
	8	0.36C	-0.21	-0.18	-0.72	0.00	-0.37			
1	6	0.68T	0.00	-1.65	-0.01	0.79	0.01	-1.15		1.89
	9	0.86C	0.00	1.53	-0.01	0.03	-0.02	@ 1.950		@ 1.840
1	6	0.00C	0.00	-5.37	0.00	2.94	0.00	-2.06		4.38
	11	0.00C	0.00	3.67	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.44T	0.00	14.56	0.03	-2.10	-0.06	14.37		13.80
	10	0.44C	0.00	-13.60	0.03	0.00	0.06	@ 2.275		@ 2.231



# WD Eng

Job No.	2466	Sheet No.	24	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (005 : Dead+Live 1.40D0+1.40D1+1.60L1+EHL@180)**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.39	0.00	0.00	0.00	0.28		0.00
	2	0.00C	0.00	-1.39	0.00	0.00	0.00	@ 0.384		@ 0.000
1	2	0.00C	0.00	0.81	0.00	0.00	0.00	0.09		0.00
	3	0.00C	0.00	-0.84	0.00	0.00	0.00	@ 0.223		@ 0.000
1	3	0.00C	0.00	4.26	0.00	0.00	0.00	2.71		0.05
	8	0.00C	0.00	-2.13	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	2.12T	0.00	3.20	0.00	-0.51	0.00	0.22	0.00	0.10
	5	2.12T	0.00	-1.35	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.81C	-0.01	0.11	0.01	0.00	-0.01	0.03		0.35
	5	2.24C	0.01	-0.56	0.01	-0.75	0.02	@ 0.536		@ 2.279
1	3	0.32C	-0.01	0.13	0.01	0.00	-0.01	0.04		0.55
	6	0.32T	0.01	-0.62	0.01	-0.91	0.04	@ 0.600		@ 2.512
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.82T	0.02	-0.56	0.95	-0.09	-0.14			0.06
	6	2.81T	-0.02	-2.61	0.95	-1.07	0.43			@ 0.371
1	5	1.61C	0.01	-1.65	0.05	0.77	-0.13	-1.05		1.79
	9	2.82C	-0.01	1.49	0.05	-0.03	0.04	@ 2.054		@ 1.845
1	6	1.62T	-0.14	3.92	-0.76	-2.66	0.70	0.72	-1.33	2.29
	7	1.25C	0.14	-1.23	-0.76	0.20	-1.33	@ 1.843	@ 2.668	@ 1.788
1	7	0.64T	0.21	1.61	-0.72	-1.18	1.31			
	8	0.36C	-0.21	-0.18	-0.72	0.00	-0.37			
1	6	0.68T	0.00	-1.65	-0.01	0.79	0.01	-1.15		1.89
	9	0.86C	0.00	1.53	-0.01	0.03	-0.02	@ 1.950		@ 1.840
1	6	0.00C	0.00	-5.37	0.00	2.94	0.00	-2.06		4.38
	11	0.00C	0.00	3.67	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.44T	0.00	14.56	0.03	-2.10	-0.06	14.37		13.80
	10	0.44C	0.00	-13.60	0.03	0.00	0.06	@ 2.275		@ 2.231

**Member Forces Ultimate (006 : Dead+Live 1.40D0+1.40D1+1.60L1+EHL@270)**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.39	0.00	0.00	0.00	0.28		0.00
	2	0.00C	0.00	-1.39	0.00	0.00	0.00	@ 0.384		@ 0.000

# WD Eng

Job No.	2466	Sheet No.	25	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (006 : Dead+Live 1.40D0+1.40D1+1.60L1+EHL@270)**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	2	0.00C	0.00	0.81	0.00	0.00	0.00	0.09		0.00
	3	0.00C	0.00	-0.84	0.00	0.00	0.00	@ 0.223		@ 0.000
1	3	0.00C	0.00	4.26	0.00	0.00	0.00	2.71		0.05
	8	0.00C	0.00	-2.13	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	2.14T	0.00	3.20	0.00	-0.51	0.00	0.22	0.00	0.10
	5	2.14T	0.00	-1.35	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.82C	-0.01	0.11	0.01	0.00	-0.01	0.03		0.35
	5	2.25C	0.01	-0.56	0.01	-0.75	0.02	@ 0.536		@ 2.279
1	3	0.32C	-0.01	0.13	0.01	0.00	-0.01	0.04		0.55
	6	0.32T	0.01	-0.62	0.01	-0.91	0.04	@ 0.600		@ 2.512
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.81T	0.02	-0.56	0.95	-0.09	-0.14			0.06
	6	2.81T	-0.02	-2.61	0.95	-1.07	0.43			@ 0.371
1	5	1.60C	0.01	-1.65	0.05	0.77	-0.13	-1.05		1.79
	9	2.80C	-0.01	1.49	0.05	-0.03	0.04	@ 2.054		@ 1.845
1	6	1.62T	-0.14	3.92	-0.76	-2.66	0.70	0.72	-1.33	2.29
	7	1.25C	0.14	-1.23	-0.76	0.20	-1.33	@ 1.843	@ 2.668	@ 1.788
1	7	0.64T	0.21	1.61	-0.72	-1.18	1.31			
	8	0.36C	-0.21	-0.18	-0.72	0.00	-0.37			
1	6	0.68T	0.00	-1.65	-0.01	0.79	0.01	-1.15		1.89
	9	0.86C	0.00	1.53	-0.01	0.03	-0.02	@ 1.950		@ 1.840
1	6	0.00C	0.00	-5.37	0.00	2.94	0.00	-2.06		4.38
	11	0.00C	0.00	3.67	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.44T	0.00	14.56	0.03	-2.10	-0.06	14.37		13.80
	10	0.44C	0.00	-13.60	0.03	0.00	0.06	@ 2.275		@ 2.231

**Member Forces Ultimate (009 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W1 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.13	0.00	0.00	0.00	0.23		0.00
	2	0.00C	0.00	-1.13	0.00	0.00	0.00	@ 0.392		@ 0.000
1	2	0.00C	0.00	0.66	0.00	0.00	0.00	0.08		0.00
	3	0.00C	0.00	-0.69	0.00	0.00	0.00	@ 0.227		@ 0.000

# WD Eng

Job No.	2466	Sheet No.	26	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (009 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W1 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	3	0.00C	0.00	3.48	0.00	0.00	0.00	2.21		0.04
	8	0.00C	0.00	-1.74	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.78T	0.00	2.61	0.00	-0.42	0.00	0.18	0.00	0.08
	5	1.78T	0.00	-1.11	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.35C	-0.01	0.10	0.01	0.00	-0.01	0.03		0.28
	5	1.86C	0.01	-0.47	0.01	-0.62	0.01	@ 0.570		@ 2.313
1	3	0.27C	0.00	0.12	0.01	0.00	-0.01	0.04		0.44
	6	0.27T	0.00	-0.52	0.01	-0.76	0.04	@ 0.637		@ 2.549
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.50T	0.02	-0.45	0.78	-0.08	-0.11			0.05
	6	2.31T	-0.02	-2.13	0.78	-0.87	0.36			@ 0.371
1	5	1.35C	0.01	-1.37	0.04	0.64	-0.11	-0.87		1.48
	9	2.35C	-0.01	1.23	0.04	-0.03	0.03	@ 2.054		@ 1.845
1	6	1.33T	-0.11	3.22	-0.62	-2.18	0.57	0.59	-1.08	1.87
	7	1.03C	0.11	-1.01	-0.62	0.16	-1.08	@ 1.843	@ 2.668	@ 1.788
1	7	0.53T	0.17	1.33	-0.59	-0.97	1.07			
	8	0.30C	-0.17	-0.16	-0.59	0.00	-0.31			
1	6	0.56T	0.00	-1.37	-0.01	0.65	0.00	-0.95		1.56
	9	0.71C	0.00	1.26	-0.01	0.02	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-4.41	0.00	2.41	0.00	-1.69		3.59
	11	0.00C	0.00	3.01	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.36T	0.00	11.90	0.02	-1.72	-0.05	11.74		11.27
	10	0.36C	0.00	-11.11	0.02	0.00	0.05	@ 2.275		@ 2.231

**Member Forces Ultimate (011 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W2 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.13	0.00	0.00	0.00	0.23		0.00
	2	0.00C	0.00	-1.13	0.00	0.00	0.00	@ 0.392		@ 0.000
1	2	0.00C	0.00	0.66	0.00	0.00	0.00	0.08		0.00
	3	0.00C	0.00	-0.69	0.00	0.00	0.00	@ 0.227		@ 0.000
1	3	0.00C	0.00	3.48	0.00	0.00	0.00	2.21		0.04
	8	0.00C	0.00	-1.74	0.00	0.00	0.00	@ 1.386		@ 1.584

# WD Eng

Job No.	2466	Sheet No.	27	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (011 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W2 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	4	1.78T	0.00	2.61	0.00	-0.42	0.00	0.18	0.00	0.08
	5	1.78T	0.00	-1.11	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.35C	-0.01	0.10	0.01	0.00	-0.01	0.03		0.28
	5	1.86C	0.01	-0.47	0.01	-0.62	0.01	@ 0.570		@ 2.313
1	3	0.27C	0.00	0.12	0.01	0.00	-0.01	0.04		0.44
	6	0.27T	0.00	-0.52	0.01	-0.76	0.04	@ 0.637		@ 2.549
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.50T	0.02	-0.45	0.78	-0.08	-0.11			0.05
	6	2.31T	-0.02	-2.13	0.78	-0.87	0.36			@ 0.371
1	5	1.35C	0.01	-1.37	0.04	0.64	-0.11	-0.87		1.48
	9	2.35C	-0.01	1.23	0.04	-0.03	0.03	@ 2.054		@ 1.845
1	6	1.33T	-0.11	3.22	-0.62	-2.18	0.57	0.59	-1.08	1.87
	7	1.03C	0.11	-1.01	-0.62	0.16	-1.08	@ 1.843	@ 2.668	@ 1.788
1	7	0.53T	0.17	1.33	-0.59	-0.97	1.07			
	8	0.30C	-0.17	-0.16	-0.59	0.00	-0.31			
1	6	0.56T	0.00	-1.37	-0.01	0.65	0.00	-0.95		1.56
	9	0.71C	0.00	1.26	-0.01	0.02	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-4.41	0.00	2.41	0.00	-1.69		3.59
	11	0.00C	0.00	3.01	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.36T	0.00	11.90	0.02	-1.72	-0.05	11.74		11.27
	10	0.36C	0.00	-11.11	0.02	0.00	0.05	@ 2.275		@ 2.231

**Member Forces Ultimate (013 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W3 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.13	0.00	0.00	0.00	0.23		0.00
	2	0.00C	0.00	-1.13	0.00	0.00	0.00	@ 0.392		@ 0.000
1	2	0.00C	0.00	0.66	0.00	0.00	0.00	0.08		0.00
	3	0.00C	0.00	-0.69	0.00	0.00	0.00	@ 0.227		@ 0.000
1	3	0.00C	0.00	3.48	0.00	0.00	0.00	2.21		0.04
	8	0.00C	0.00	-1.74	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.78T	0.00	2.61	0.00	-0.42	0.00	0.18	0.00	0.08
	5	1.78T	0.00	-1.11	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464

# WD Eng

Job No.	2466	Sheet No.	28	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (013 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W3 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.35C	-0.01	0.10	0.01	0.00	-0.01	0.03		0.28
	5	1.86C	0.01	-0.47	0.01	-0.62	0.01	@ 0.570		@ 2.313
1	3	0.27C	0.00	0.12	0.01	0.00	-0.01	0.04		0.44
	6	0.27T	0.00	-0.52	0.01	-0.76	0.04	@ 0.637		@ 2.549
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.50T	0.02	-0.45	0.78	-0.08	-0.11			0.05
	6	2.31T	-0.02	-2.13	0.78	-0.87	0.36			@ 0.371
1	5	1.35C	0.01	-1.37	0.04	0.64	-0.11	-0.87		1.48
	9	2.35C	-0.01	1.23	0.04	-0.03	0.03	@ 2.054		@ 1.845
1	6	1.33T	-0.11	3.22	-0.62	-2.18	0.57	0.59	-1.08	1.87
	7	1.03C	0.11	-1.01	-0.62	0.16	-1.08	@ 1.843	@ 2.668	@ 1.788
1	7	0.53T	0.17	1.33	-0.59	-0.97	1.07			
	8	0.30C	-0.17	-0.16	-0.59	0.00	-0.31			
1	6	0.56T	0.00	-1.37	-0.01	0.65	0.00	-0.95		1.56
	9	0.71C	0.00	1.26	-0.01	0.02	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-4.41	0.00	2.41	0.00	-1.69		3.59
	11	0.00C	0.00	3.01	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.36T	0.00	11.90	0.02	-1.72	-0.05	11.74		11.27
	10	0.36C	0.00	-11.11	0.02	0.00	0.05	@ 2.275		@ 2.231

**Member Forces Ultimate (015 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W4 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.13	0.00	0.00	0.00	0.23		0.00
	2	0.00C	0.00	-1.13	0.00	0.00	0.00	@ 0.392		@ 0.000
1	2	0.00C	0.00	0.66	0.00	0.00	0.00	0.08		0.00
	3	0.00C	0.00	-0.69	0.00	0.00	0.00	@ 0.227		@ 0.000
1	3	0.00C	0.00	3.48	0.00	0.00	0.00	2.21		0.04
	8	0.00C	0.00	-1.74	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.78T	0.00	2.61	0.00	-0.42	0.00	0.18	0.00	0.08
	5	1.78T	0.00	-1.11	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000

# WD Eng

Job No.	2466	Sheet No.	29	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (015 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W4 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	2	2.35C	-0.01	0.10	0.01	0.00	-0.01	0.03		0.28
	5	1.86C	0.01	-0.47	0.01	-0.62	0.01	@ 0.570		@ 2.313
1	3	0.27C	0.00	0.12	0.01	0.00	-0.01	0.04		0.44
	6	0.27T	0.00	-0.52	0.01	-0.76	0.04	@ 0.637		@ 2.549
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.50T	0.02	-0.45	0.78	-0.08	-0.11			0.05
	6	2.31T	-0.02	-2.13	0.78	-0.87	0.36			@ 0.371
1	5	1.35C	0.01	-1.37	0.04	0.64	-0.11	-0.87		1.48
	9	2.35C	-0.01	1.23	0.04	-0.03	0.03	@ 2.054		@ 1.845
1	6	1.33T	-0.11	3.22	-0.62	-2.18	0.57	0.59	-1.08	1.87
	7	1.03C	0.11	-1.01	-0.62	0.16	-1.08	@ 1.843	@ 2.668	@ 1.788
1	7	0.53T	0.17	1.33	-0.59	-0.97	1.07			
	8	0.30C	-0.17	-0.16	-0.59	0.00	-0.31			
1	6	0.56T	0.00	-1.37	-0.01	0.65	0.00	-0.95		1.56
	9	0.71C	0.00	1.26	-0.01	0.02	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-4.41	0.00	2.41	0.00	-1.69		3.59
	11	0.00C	0.00	3.01	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.36T	0.00	11.90	0.02	-1.72	-0.05	11.74		11.27
	10	0.36C	0.00	-11.11	0.02	0.00	0.05	@ 2.275		@ 2.231

**Member Forces Ultimate (017 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W5 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.13	0.00	0.00	0.00	0.23		0.00
	2	0.00C	0.00	-1.13	0.00	0.00	0.00	@ 0.392		@ 0.000
1	2	0.00C	0.00	0.66	0.00	0.00	0.00	0.08		0.00
	3	0.00C	0.00	-0.69	0.00	0.00	0.00	@ 0.227		@ 0.000
1	3	0.00C	0.00	3.48	0.00	0.00	0.00	2.21		0.04
	8	0.00C	0.00	-1.74	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.78T	0.00	2.61	0.00	-0.42	0.00	0.18	0.00	0.08
	5	1.78T	0.00	-1.11	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.35C	-0.01	0.10	0.01	0.00	-0.01	0.03		0.28
	5	1.86C	0.01	-0.47	0.01	-0.62	0.01	@ 0.570		@ 2.313

# WD Eng

Job No.	2466	Sheet No.	30	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (017 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W5 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	3	0.27C	0.00	0.12	0.01	0.00	-0.01	0.04		0.44
	6	0.27T	0.00	-0.52	0.01	-0.76	0.04	@ 0.637		@ 2.549
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.50T	0.02	-0.45	0.78	-0.08	-0.11			0.05
	6	2.31T	-0.02	-2.13	0.78	-0.87	0.36			@ 0.371
1	5	1.35C	0.01	-1.37	0.04	0.64	-0.11	-0.87		1.48
	9	2.35C	-0.01	1.23	0.04	-0.03	0.03	@ 2.054		@ 1.845
1	6	1.33T	-0.11	3.22	-0.62	-2.18	0.57	0.59	-1.08	1.87
	7	1.03C	0.11	-1.01	-0.62	0.16	-1.08	@ 1.843	@ 2.668	@ 1.788
1	7	0.53T	0.17	1.33	-0.59	-0.97	1.07			
	8	0.30C	-0.17	-0.16	-0.59	0.00	-0.31			
1	6	0.56T	0.00	-1.37	-0.01	0.65	0.00	-0.95		1.56
	9	0.71C	0.00	1.26	-0.01	0.02	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-4.41	0.00	2.41	0.00	-1.69		3.59
	11	0.00C	0.00	3.01	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.36T	0.00	11.90	0.02	-1.72	-0.05	11.74		11.27
	10	0.36C	0.00	-11.11	0.02	0.00	0.05	@ 2.275		@ 2.231

**Member Forces Ultimate (019 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W6 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.13	0.00	0.00	0.00	0.23		0.00
	2	0.00C	0.00	-1.13	0.00	0.00	0.00	@ 0.392		@ 0.000
1	2	0.00C	0.00	0.66	0.00	0.00	0.00	0.08		0.00
	3	0.00C	0.00	-0.69	0.00	0.00	0.00	@ 0.227		@ 0.000
1	3	0.00C	0.00	3.48	0.00	0.00	0.00	2.21		0.04
	8	0.00C	0.00	-1.74	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.78T	0.00	2.61	0.00	-0.42	0.00	0.18	0.00	0.08
	5	1.78T	0.00	-1.11	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.35C	-0.01	0.10	0.01	0.00	-0.01	0.03		0.28
	5	1.86C	0.01	-0.47	0.01	-0.62	0.01	@ 0.570		@ 2.313
1	3	0.27C	0.00	0.12	0.01	0.00	-0.01	0.04		0.44
	6	0.27T	0.00	-0.52	0.01	-0.76	0.04	@ 0.637		@ 2.549

# WD Eng

Job No.	2466	Sheet No.	31	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (019 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W6 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.50T	0.02	-0.45	0.78	-0.08	-0.11			0.05
	6	2.31T	-0.02	-2.13	0.78	-0.87	0.36			@ 0.371
1	5	1.35C	0.01	-1.37	0.04	0.64	-0.11	-0.87		1.48
	9	2.35C	-0.01	1.23	0.04	-0.03	0.03	@ 2.054		@ 1.845
1	6	1.33T	-0.11	3.22	-0.62	-2.18	0.57	0.59	-1.08	1.87
	7	1.03C	0.11	-1.01	-0.62	0.16	-1.08	@ 1.843	@ 2.668	@ 1.788
1	7	0.53T	0.17	1.33	-0.59	-0.97	1.07			
	8	0.30C	-0.17	-0.16	-0.59	0.00	-0.31			
1	6	0.56T	0.00	-1.37	-0.01	0.65	0.00	-0.95		1.56
	9	0.71C	0.00	1.26	-0.01	0.02	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-4.41	0.00	2.41	0.00	-1.69		3.59
	11	0.00C	0.00	3.01	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.36T	0.00	11.90	0.02	-1.72	-0.05	11.74		11.27
	10	0.36C	0.00	-11.11	0.02	0.00	0.05	@ 2.275		@ 2.231

**Member Forces Ultimate (021 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W7 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.13	0.00	0.00	0.00	0.23		0.00
	2	0.00C	0.00	-1.13	0.00	0.00	0.00	@ 0.392		@ 0.000
1	2	0.00C	0.00	0.66	0.00	0.00	0.00	0.08		0.00
	3	0.00C	0.00	-0.69	0.00	0.00	0.00	@ 0.227		@ 0.000
1	3	0.00C	0.00	3.48	0.00	0.00	0.00	2.21		0.04
	8	0.00C	0.00	-1.74	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.78T	0.00	2.61	0.00	-0.42	0.00	0.18	0.00	0.08
	5	1.78T	0.00	-1.11	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.35C	-0.01	0.10	0.01	0.00	-0.01	0.03		0.28
	5	1.86C	0.01	-0.47	0.01	-0.62	0.01	@ 0.570		@ 2.313
1	3	0.27C	0.00	0.12	0.01	0.00	-0.01	0.04		0.44
	6	0.27T	0.00	-0.52	0.01	-0.76	0.04	@ 0.637		@ 2.549
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000



# WD Eng

Job No.	2466	Sheet No.	32	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (021 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W7 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	5	1.50T	0.02	-0.45	0.78	-0.08	-0.11			0.05
	6	2.31T	-0.02	-2.13	0.78	-0.87	0.36			@ 0.371
1	5	1.35C	0.01	-1.37	0.04	0.64	-0.11	-0.87		1.48
	9	2.35C	-0.01	1.23	0.04	-0.03	0.03	@ 2.054		@ 1.845
1	6	1.33T	-0.11	3.22	-0.62	-2.18	0.57	0.59	-1.08	1.87
	7	1.03C	0.11	-1.01	-0.62	0.16	-1.08	@ 1.843	@ 2.668	@ 1.788
1	7	0.53T	0.17	1.33	-0.59	-0.97	1.07			
	8	0.30C	-0.17	-0.16	-0.59	0.00	-0.31			
1	6	0.56T	0.00	-1.37	-0.01	0.65	0.00	-0.95		1.56
	9	0.71C	0.00	1.26	-0.01	0.02	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-4.41	0.00	2.41	0.00	-1.69		3.59
	11	0.00C	0.00	3.01	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.36T	0.00	11.90	0.02	-1.72	-0.05	11.74		11.27
	10	0.36C	0.00	-11.11	0.02	0.00	0.05	@ 2.275		@ 2.231

**Member Forces Ultimate (023 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W8 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.13	0.00	0.00	0.00	0.23		0.00
	2	0.00C	0.00	-1.13	0.00	0.00	0.00	@ 0.392		@ 0.000
1	2	0.00C	0.00	0.66	0.00	0.00	0.00	0.08		0.00
	3	0.00C	0.00	-0.69	0.00	0.00	0.00	@ 0.227		@ 0.000
1	3	0.00C	0.00	3.48	0.00	0.00	0.00	2.21		0.04
	8	0.00C	0.00	-1.74	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.78T	0.00	2.61	0.00	-0.42	0.00	0.18	0.00	0.08
	5	1.78T	0.00	-1.11	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.35C	-0.01	0.10	0.01	0.00	-0.01	0.03		0.28
	5	1.86C	0.01	-0.47	0.01	-0.62	0.01	@ 0.570		@ 2.313
1	3	0.27C	0.00	0.12	0.01	0.00	-0.01	0.04		0.44
	6	0.27T	0.00	-0.52	0.01	-0.76	0.04	@ 0.637		@ 2.549
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.50T	0.02	-0.45	0.78	-0.08	-0.11			0.05
	6	2.31T	-0.02	-2.13	0.78	-0.87	0.36			@ 0.371

# WD Eng

Job No.	2466	Sheet No.	33	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (023 : Dead+ Live+Wind 1.20D0+1.20D1+1.20L1+1.20W8 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	5	1.35C	0.01	-1.37	0.04	0.64	-0.11	-0.87		1.48
	9	2.35C	-0.01	1.23	0.04	-0.03	0.03	@ 2.054		@ 1.845
1	6	1.33T	-0.11	3.22	-0.62	-2.18	0.57	0.59	-1.08	1.87
	7	1.03C	0.11	-1.01	-0.62	0.16	-1.08	@ 1.843	@ 2.668	@ 1.788
1	7	0.53T	0.17	1.33	-0.59	-0.97	1.07			
	8	0.30C	-0.17	-0.16	-0.59	0.00	-0.31			
1	6	0.56T	0.00	-1.37	-0.01	0.65	0.00	-0.95		1.56
	9	0.71C	0.00	1.26	-0.01	0.02	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-4.41	0.00	2.41	0.00	-1.69		3.59
	11	0.00C	0.00	3.01	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.36T	0.00	11.90	0.02	-1.72	-0.05	11.74		11.27
	10	0.36C	0.00	-11.11	0.02	0.00	0.05	@ 2.275		@ 2.231

**Member Forces Ultimate (025 : Dead+Wind 1.00D0+1.00D1+1.40W1 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.12	0.00	0.00	-0.01	0.05		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.771		@ 2.480
1	3	0.23C	0.00	0.13	0.01	0.00	0.00	0.06		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.900		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845

# WD Eng

Job No.	2466	Sheet No.	34	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (025 : Dead+Wind 1.00D0+1.00D1+1.40W1 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231

**Member Forces Ultimate (027 : Dead+Wind 1.00D0+1.00D1+1.40W2 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.12	0.00	0.00	-0.01	0.05		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.771		@ 2.480
1	3	0.23C	0.00	0.13	0.01	0.00	0.00	0.06		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.900		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788

# WD Eng

Job No.	2466	Sheet No.	35	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (027 : Dead+Wind 1.00D0+1.00D1+1.40W2 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231

**Member Forces Ultimate (029 : Dead+Wind 1.00D0+1.00D1+1.40W3 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.12	0.00	0.00	-0.01	0.05		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.771		@ 2.480
1	3	0.23C	0.00	0.13	0.01	0.00	0.00	0.06		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.900		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			

# WD Eng

Job No.	2466	Sheet No.	36	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (029 : Dead+Wind 1.00D0+1.00D1+1.40W3 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231

**Member Forces Ultimate (031 : Dead+Wind 1.00D0+1.00D1+1.40W4 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.12	0.00	0.00	-0.01	0.05		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.771		@ 2.480
1	3	0.23C	0.00	0.13	0.01	0.00	0.00	0.06		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.900		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840

# WD Eng

Job No.	2466	Sheet No.	37	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (031 : Dead+Wind 1.00D0+1.00D1+1.40W4 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231

**Member Forces Ultimate (033 : Dead+Wind 1.00D0+1.00D1+1.40W5 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.12	0.00	0.00	-0.01	0.05		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.771		@ 2.480
1	3	0.23C	0.00	0.13	0.01	0.00	0.00	0.06		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.900		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687

# WD Eng

Job No.	2466	Sheet No.	38	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (033 : Dead+Wind 1.00D0+1.00D1+1.40W5 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231

**Member Forces Ultimate (035 : Dead+Wind 1.00D0+1.00D1+1.40W6 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.12	0.00	0.00	-0.01	0.05		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.771		@ 2.480
1	3	0.23C	0.00	0.13	0.01	0.00	0.00	0.06		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.900		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000

# WD Eng

Job No.	2466	Sheet No.	39	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (035 : Dead+Wind 1.00D0+1.00D1+1.40W6 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231

**Member Forces Ultimate (037 : Dead+Wind 1.00D0+1.00D1+1.40W7 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.12	0.00	0.00	-0.01	0.05		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.771		@ 2.480
1	3	0.23C	0.00	0.13	0.01	0.00	0.00	0.06		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.900		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231



# WD Eng

Job No.	2466	Sheet No.	40	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

**Member Forces Ultimate (039 : Dead+Wind 1.00D0+1.00D1+1.40W8 (Ultimate))**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.12	0.00	0.00	-0.01	0.05		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.771		@ 2.480
1	3	0.23C	0.00	0.13	0.01	0.00	0.00	0.06		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.900		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231

**Member Forces Ultimate (Maximum Values)**

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	1.39	0.00	0.00	0.00	0.28		0.00
	2	0.00C	0.00	-1.39	0.00	0.00	0.00	@ 0.384		@ 0.000

# WD Eng

Job No.	2466	Sheet No.	41	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Member Forces Ultimate (Maximum Values)

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	2	0.00C	0.00	0.81	0.00	0.00	0.00	0.09		0.00
	3	0.00C	0.00	-0.84	0.00	0.00	0.00	@ 0.223		@ 0.000
1	3	0.00C	0.00	4.26	0.00	0.00	0.00	2.71		0.05
	8	0.00C	0.00	-2.13	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	2.15T	0.00	3.20	0.00	-0.51	0.00	0.22	0.00	0.10
	5	2.15T	0.00	-1.35	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.464
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	2.82C	-0.01	0.12	0.01	0.00	-0.01	0.05		0.35
	5	2.25C	0.01	-0.56	0.01	-0.75	0.02	@ 0.771		@ 2.279
1	3	0.32C	-0.01	0.13	0.01	0.00	-0.01	0.06		0.55
	6	0.32T	0.01	-0.62	0.01	-0.91	0.04	@ 0.900		@ 2.512
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	1.82T	0.02	-0.56	0.95	-0.09	-0.14			0.06
	6	2.81T	-0.02	-2.61	0.95	-1.07	0.43			@ 0.371
1	5	1.63C	0.01	-1.65	0.05	0.77	-0.13	-1.05		1.79
	9	2.84C	-0.01	1.49	0.05	-0.03	0.04	@ 2.054		@ 1.845
1	6	1.62T	-0.14	3.92	-0.76	-2.66	0.70	0.72	-1.33	2.29
	7	1.25C	0.14	-1.23	-0.76	0.20	-1.33	@ 1.843	@ 2.668	@ 1.788
1	7	0.64T	0.21	1.61	-0.72	-1.18	1.31			
	8	0.36C	-0.21	-0.18	-0.72	0.00	-0.37			
1	6	0.68T	0.00	-1.65	-0.01	0.79	0.01	-1.15		1.89
	9	0.86C	0.00	1.53	-0.01	0.03	-0.02	@ 1.950		@ 1.840
1	6	0.00C	0.00	-5.37	0.00	2.94	0.00	-2.06		4.38
	11	0.00C	0.00	3.67	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	-0.01	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.44T	0.00	14.56	0.03	-2.10	-0.06	14.37		13.80
	10	0.44C	0.00	-13.60	0.03	0.00	0.06	@ 2.275		@ 2.231

### Member Forces Ultimate (Minimum Values)

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	1	0.00C	0.00	0.61	0.00	0.00	0.00	0.12		0.00
	2	0.00C	0.00	-0.61	0.00	0.00	0.00	@ 0.376		@ 0.000
1	2	0.00C	0.00	0.36	0.00	0.00	0.00	0.04		0.00
	3	0.00C	0.00	-0.37	0.00	0.00	0.00	@ 0.209		@ 0.000

# WD Eng

Job No.	2466	Sheet No.	42	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Member Forces Ultimate (Minimum Values)

Load Case	Node End1 End2	Axial Force (kN)	Torque Moment (kNm)	Shear Force (kN)		Bending Moment (kNm)		Maximum Moment (kNm @ m)		Max Def (mm @ m)
				x-x	y-y	x-x	y-y	x-x	y-y	
1	3	0.00C	0.00	1.88	0.00	0.00	0.00	1.19		0.02
	8	0.00C	0.00	-0.94	0.00	0.00	0.00	@ 1.386		@ 1.584
1	4	1.17T	0.00	1.43	0.00	-0.23	0.00	0.10	0.00	0.04
	5	1.17T	0.00	-0.60	0.00	0.00	0.00	@ 0.480	@ 0.000	@ 0.472
1	1	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	4	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	2	1.56C	-0.01	0.10	0.00	0.00	-0.01	0.03		0.13
	5	1.16C	0.01	-0.36	0.00	-0.42	0.01	@ 0.570		@ 2.480
1	3	0.23C	0.00	0.12	0.01	0.00	0.00	0.04		0.21
	6	0.23T	0.00	-0.40	0.01	-0.50	0.02	@ 0.637		@ 2.737
1	4	0.00C	0.00	0.00	0.00	0.00	0.00			0.00
	9	0.00C	0.00	0.00	0.00	0.00	0.00			@ 0.000
1	5	0.96T	0.01	-0.19	0.45	-0.06	-0.06			0.03
	6	1.42T	-0.01	-1.14	0.45	-0.47	0.20			@ 0.371
1	5	0.96C	0.00	-0.87	0.02	0.42	-0.06	-0.53		0.89
	9	1.58C	0.00	0.75	0.02	-0.01	0.02	@ 2.054		@ 1.845
1	6	0.76T	-0.06	1.83	-0.34	-1.24	0.31	0.33	-0.59	1.03
	7	0.60C	0.06	-0.61	-0.34	0.06	-0.59	@ 1.816	@ 2.668	@ 1.788
1	7	0.32T	0.09	0.80	-0.32	-0.56	0.59			
	8	0.20C	-0.09	-0.14	-0.32	0.00	-0.17			
1	6	0.36T	0.00	-0.87	0.00	0.43	0.00	-0.57		0.92
	9	0.43C	0.00	0.76	0.00	0.01	-0.01	@ 1.950		@ 1.840
1	6	0.00C	0.00	-2.50	0.00	1.37	0.00	-0.96		2.03
	11	0.00C	0.00	1.70	0.00	0.00	0.00	@ 1.806		@ 1.687
1	9	0.00C	0.00	0.00	0.00	0.00	0.00	0.00		0.00
	11	0.00C	0.00	0.00	0.00	0.00	0.00	@ 0.000		@ 0.000
1	7	0.20T	0.00	6.53	0.01	-0.94	-0.03	6.44		6.18
	10	0.20C	0.00	-6.10	0.01	0.00	0.03	@ 2.275		@ 2.231

### Support Reactions Serviceability (002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kNm)	My ↑ (kNm)	Mz ↗ (kNm)
1-1	0.000	0.944	0.000	0.000	0.000	0.000
2-1	0.000	2.828	1.433	0.000	-0.012	0.000
3-1	0.000	3.697	0.109	0.000	0.000	0.000
4-1	-1.482	2.176	0.000	0.000	0.000	0.347
6-1	1.054	10.702	-0.662	0.000	0.165	0.000
7-1	-0.142	12.257	0.149	0.000	1.408	0.000
8-1	0.205	1.685	0.474	0.000	0.292	0.000
9-1	0.361	2.871	-1.492	0.000	0.019	0.000
10-1	0.019	9.267	-0.010	0.000	-0.040	0.000
11-1	0.000	2.522	0.000	0.000	0.000	0.000

# W D Ceng

Job No.	2466	Sheet No.	43	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Support Reactions Serviceability (002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.944	0.000	0.000	0.000	0.000
Total	0.015	48.949	0.000	0.000	1.831	0.347

### Support Reactions Serviceability (007 : Live Only 1.00L1 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.332	0.000	0.000	0.000	0.000
2-1	0.000	0.756	0.318	0.000	0.000	0.000
3-1	0.000	1.194	0.022	0.000	0.000	0.000
4-1	-0.316	0.749	0.000	0.000	0.000	0.116
6-1	0.229	3.201	-0.284	0.000	0.064	0.000
7-1	-0.050	4.045	0.053	0.000	0.481	0.000
8-1	0.074	0.528	0.158	0.000	0.099	0.000
9-1	0.061	0.724	-0.263	0.000	0.000	0.000
10-1	0.000	3.168	0.000	0.000	-0.014	0.000
11-1	0.000	0.811	0.000	0.000	0.000	0.000
Total	-0.002	15.508	0.004	0.000	0.631	0.116

### Support Reactions Serviceability (008 : Dead Only 1.00D0+1.00D1 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (010 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W1 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
2-1	0.000	2.677	1.370	0.000	-0.012	0.000
3-1	0.000	3.458	0.105	0.000	0.000	0.000
4-1	-1.418	2.026	0.000	0.000	0.000	0.323
6-1	1.008	10.062	-0.605	0.000	0.152	0.000
7-1	-0.132	11.448	0.138	0.000	1.312	0.000
8-1	0.190	1.579	0.442	0.000	0.272	0.000
9-1	0.349	2.726	-1.439	0.000	0.018	0.000
10-1	0.017	8.633	0.000	0.000	-0.037	0.000
11-1	0.000	2.360	0.000	0.000	0.000	0.000
Total	0.014	45.848	0.010	0.000	1.705	0.323

### Support Reactions Serviceability (012 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W2 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
2-1	0.000	2.677	1.370	0.000	-0.012	0.000
3-1	0.000	3.458	0.105	0.000	0.000	0.000

# WD CEng

Job No.	2466	Sheet No.	44	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Support Reactions Serviceability (012 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W2 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
4-1	-1.418	2.026	0.000	0.000	0.000	0.323
6-1	1.008	10.062	-0.605	0.000	0.152	0.000
7-1	-0.132	11.448	0.138	0.000	1.312	0.000
8-1	0.190	1.579	0.442	0.000	0.272	0.000
9-1	0.349	2.726	-1.439	0.000	0.018	0.000
10-1	0.017	8.633	0.000	0.000	-0.037	0.000
11-1	0.000	2.360	0.000	0.000	0.000	0.000
Total	0.014	45.848	0.010	0.000	1.705	0.323

### Support Reactions Serviceability (014 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W3 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
2-1	0.000	2.677	1.370	0.000	-0.012	0.000
3-1	0.000	3.458	0.105	0.000	0.000	0.000
4-1	-1.418	2.026	0.000	0.000	0.000	0.323
6-1	1.008	10.062	-0.605	0.000	0.152	0.000
7-1	-0.132	11.448	0.138	0.000	1.312	0.000
8-1	0.190	1.579	0.442	0.000	0.272	0.000
9-1	0.349	2.726	-1.439	0.000	0.018	0.000
10-1	0.017	8.633	0.000	0.000	-0.037	0.000
11-1	0.000	2.360	0.000	0.000	0.000	0.000
Total	0.014	45.848	0.010	0.000	1.705	0.323

### Support Reactions Serviceability (016 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W4 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
2-1	0.000	2.677	1.370	0.000	-0.012	0.000
3-1	0.000	3.458	0.105	0.000	0.000	0.000
4-1	-1.418	2.026	0.000	0.000	0.000	0.323
6-1	1.008	10.062	-0.605	0.000	0.152	0.000
7-1	-0.132	11.448	0.138	0.000	1.312	0.000
8-1	0.190	1.579	0.442	0.000	0.272	0.000
9-1	0.349	2.726	-1.439	0.000	0.018	0.000
10-1	0.017	8.633	0.000	0.000	-0.037	0.000
11-1	0.000	2.360	0.000	0.000	0.000	0.000
Total	0.014	45.848	0.010	0.000	1.705	0.323

### Support Reactions Serviceability (018 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W5 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
2-1	0.000	2.677	1.370	0.000	-0.012	0.000
3-1	0.000	3.458	0.105	0.000	0.000	0.000
4-1	-1.418	2.026	0.000	0.000	0.000	0.323
6-1	1.008	10.062	-0.605	0.000	0.152	0.000
7-1	-0.132	11.448	0.138	0.000	1.312	0.000
8-1	0.190	1.579	0.442	0.000	0.272	0.000
9-1	0.349	2.726	-1.439	0.000	0.018	0.000
10-1	0.017	8.633	0.000	0.000	-0.037	0.000
11-1	0.000	2.360	0.000	0.000	0.000	0.000
Total	0.014	45.848	0.010	0.000	1.705	0.323

# W D Ceng

Job No.	2466	Sheet No.	45	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Support Reactions Serviceability (020 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W6 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
2-1	0.000	2.677	1.370	0.000	-0.012	0.000
3-1	0.000	3.458	0.105	0.000	0.000	0.000
4-1	-1.418	2.026	0.000	0.000	0.000	0.323
6-1	1.008	10.062	-0.605	0.000	0.152	0.000
7-1	-0.132	11.448	0.138	0.000	1.312	0.000
8-1	0.190	1.579	0.442	0.000	0.272	0.000
9-1	0.349	2.726	-1.439	0.000	0.018	0.000
10-1	0.017	8.633	0.000	0.000	-0.037	0.000
11-1	0.000	2.360	0.000	0.000	0.000	0.000
Total	0.014	45.848	0.010	0.000	1.705	0.323

### Support Reactions Serviceability (022 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W7 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
2-1	0.000	2.677	1.370	0.000	-0.012	0.000
3-1	0.000	3.458	0.105	0.000	0.000	0.000
4-1	-1.418	2.026	0.000	0.000	0.000	0.323
6-1	1.008	10.062	-0.605	0.000	0.152	0.000
7-1	-0.132	11.448	0.138	0.000	1.312	0.000
8-1	0.190	1.579	0.442	0.000	0.272	0.000
9-1	0.349	2.726	-1.439	0.000	0.018	0.000
10-1	0.017	8.633	0.000	0.000	-0.037	0.000
11-1	0.000	2.360	0.000	0.000	0.000	0.000
Total	0.014	45.848	0.010	0.000	1.705	0.323

### Support Reactions Serviceability (024 : Dead+ Live+Wind 1.00D0+1.00D1+0.80L1+0.80W8 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.877	0.000	0.000	0.000	0.000
2-1	0.000	2.677	1.370	0.000	-0.012	0.000
3-1	0.000	3.458	0.105	0.000	0.000	0.000
4-1	-1.418	2.026	0.000	0.000	0.000	0.323
6-1	1.008	10.062	-0.605	0.000	0.152	0.000
7-1	-0.132	11.448	0.138	0.000	1.312	0.000
8-1	0.190	1.579	0.442	0.000	0.272	0.000
9-1	0.349	2.726	-1.439	0.000	0.018	0.000
10-1	0.017	8.633	0.000	0.000	-0.037	0.000
11-1	0.000	2.360	0.000	0.000	0.000	0.000
Total	0.014	45.848	0.010	0.000	1.705	0.323

### Support Reactions Serviceability (026 : Dead+Wind 1.00D0+1.00D1+1.00W1 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000

# WD eng

Job No.	2466	Sheet No.	46	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Support Reactions Serviceability (026 : Dead+Wind 1.00D0+1.00D1+1.00W1 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (028 : Dead+Wind 1.00D0+1.00D1+1.00W2 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (030 : Dead+Wind 1.00D0+1.00D1+1.00W3 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (032 : Dead+Wind 1.00D0+1.00D1+1.00W4 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (034 : Dead+Wind 1.00D0+1.00D1+1.00W5 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000

# WD Eng

Job No.	2466	Sheet No.	47	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Support Reactions Serviceability (034 : Dead+Wind 1.00D0+1.00D1+1.00W5 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (036 : Dead+Wind 1.00D0+1.00D1+1.00W6 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (038 : Dead+Wind 1.00D0+1.00D1+1.00W7 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (040 : Dead+Wind 1.00D0+1.00D1+1.00W8 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
2-1	0.000	2.072	1.115	0.000	0.000	0.000
3-1	0.000	2.503	0.087	0.000	0.000	0.000
4-1	-1.165	1.427	0.000	0.000	0.000	0.231
6-1	0.825	7.501	-0.378	0.000	0.101	0.000
7-1	-0.091	8.212	0.095	0.000	0.927	0.000
8-1	0.131	1.157	0.316	0.000	0.192	0.000
9-1	0.299	2.147	-1.229	0.000	0.015	0.000
10-1	0.012	6.099	0.000	0.000	-0.026	0.000
11-1	0.000	1.711	0.000	0.000	0.000	0.000



# WD CEng

Job No.	2466	Sheet No.	48	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

### Support Reactions Serviceability (040 : Dead+Wind 1.00D0+1.00D1+1.00W8 (Serviceability))

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.612	0.000	0.000	0.000	0.000
Total	0.011	33.441	0.007	0.000	1.209	0.231

### Support Reactions Serviceability (Maximum Values)

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.944	0.000	0.000	0.000	0.000
2-1	0.000	2.828	1.433	0.000	-0.012	0.000
3-1	0.000	3.697	0.109	0.000	0.000	0.000
4-1	-1.482	2.176	0.000	0.000	0.000	0.347
6-1	1.054	10.702	-0.662	0.000	0.165	0.000
7-1	-0.142	12.257	0.149	0.000	1.408	0.000
8-1	0.205	1.685	0.474	0.000	0.292	0.000
9-1	0.361	2.871	-1.492	0.000	0.019	0.000
10-1	0.019	9.267	-0.010	0.000	-0.040	0.000
11-1	0.000	2.522	0.000	0.000	0.000	0.000
Total	0.015	48.949	0.010	0.000	1.831	0.347

### Support Reactions Serviceability (Minimum Values)

Load Case	Directional Reactions (kN)			Moment Reactions (kNm)		
	Rx → (kN)	Ry ↑ (kN)	Rz ↗ (kN)	Mx → (kN)	My ↑ (kN)	Mz ↗ (kN)
1-1	0.000	0.332	0.000	0.000	0.000	0.000
2-1	0.000	0.756	0.318	0.000	0.000	0.000
3-1	0.000	1.194	0.022	0.000	0.000	0.000
4-1	-0.316	0.749	0.000	0.000	0.000	0.116
6-1	0.229	3.201	-0.284	0.000	0.064	0.000
7-1	-0.050	4.045	0.053	0.000	0.481	0.000
8-1	0.074	0.528	0.158	0.000	0.099	0.000
9-1	0.061	0.724	-0.263	0.000	0.000	0.000
10-1	0.000	3.168	0.000	0.000	-0.014	0.000
11-1	0.000	0.811	0.000	0.000	0.000	0.000
Total	-0.002	15.508	0.000	0.000	0.631	0.116

# WD Eng

Job No.	2466	Sheet No.	49	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

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## MASTERKEY : TIMBER DESIGN

### AXIAL LOAD WITH MOMENT DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 2 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 38, h = 147, 147x38 in Strength Class C24, No wane at bearing
Section Properties (c,cm <sup>3</sup> ,cm)	Area 55.9, Zx 136.9, Zy 35.4, rx 4.24, ry 1.1
Specification	1 : Internal use in continuously heated building Long term loading
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Member Details	F = -1.482 kN, L = 0.8 m, Lx = 0.8 m, Ly = 0.8 m, Lex = 1.0 Lx, Ley = 1.0 Ly Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{mx.adm} = K_2.K_3.K_{7x}.K_8.\sigma_m$	1.00 x 1.00 x 1.08 x 1.00 x 7.50	8.11 N/mm <sup>2</sup>
$\sigma_{my.adm} = K_2.K_3.K_{7y}.K_8.\sigma_m$	1.00 x 1.00 x 1.17 x 1.00 x 7.50	8.78 N/mm <sup>2</sup>
$\sigma_{t.adm} = K_2.K_3.K_8.K_{14}.\sigma_t$	1.00 x 1.00 x 1.00 x 1.08 x 4.50	4.87 N/mm <sup>2</sup>
$\sigma_{c\perp.adm} = K_2.K_3.K_4.K_8.\sigma_{c\perp}$	1.00 x 1.00 x 1.14 x 1.00 x 2.40	2.74 N/mm <sup>2</sup>
$T_{adm} = K_2.K_3.K_8.T$	1.00 x 1.00 x 1.00 x 0.71	0.71 N/mm <sup>2</sup>
$E = K_2.E_{mean}$	1.00 x 10800	10800.0 N/mm <sup>2</sup>

#### Tensile Resistance

$\sigma_{t.a} = F/Area$	1.482 / 55.86 ≤ 4.87	0.27 N/mm <sup>2</sup>	OK
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#### Axial Load with Moments Check

Critical Design Location	X = 0.000		
$\sigma_{mx.a} = Mx/Zx$	0.347 / 136.86 ≤ 8.11	2.54 N/mm <sup>2</sup>	OK
$\sigma_t/\sigma_{t.adm} + \sigma_{mx}/\sigma_{mx.adm}$	0.27/4.87+2.54/8.11	0.368	OK

#### Shear and Bearing Check

Critical Design Location	X = 0.000		
$T_a = 1.5 F_v / Area$	1.5 x 2.176 / 55.86 ≤ 0.71	0.58 N/mm <sup>2</sup>	OK
$\sigma_{c\perp.ax} = F_vx / (b.Bx)$	2.176 / (38 x 75) ≤ 2.74	0.76 N/mm <sup>2</sup>	OK

#### Deflection Check (Shear Deflection NOT Included)

Critical Load Case 002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)			
$\delta = \delta_m$	In-span 0.07 ≤ L/333	0.07 mm	OK

# WD Eng

Job No.	2466	Sheet No.	50	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Job Title.	47a Market Jew Street, Penzance						
Member.	Proposed room in the extension						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

## MASTERKEY : TIMBER DESIGN

### AXIAL LOAD WITH MOMENT DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 12 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 94, h = 200, 200x94 in Strength Class C24, No wane at bearing
Section Properties (c,cm <sup>3</sup> ,cm)	Area 188, Zx 626.7, Zy 294.5, rx 5.77, ry 2.71
Specification	1 : Internal use in continuously heated building Long term loading, 2 pieces of softwood, Load sharing
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Member Details	F = 1.956 kN, L = 3.352 m, Lx = 3.352 m, Ly = 3.352 m, Lex = 1.0 Lx, Ley = 1.0 Ly Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{mx,adm} = K_2 \cdot K_3 \cdot K_{7x} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.05 \times 1.10 \times 7.50$	8.63 N/mm <sup>2</sup>
$\sigma_{my,adm} = K_2 \cdot K_3 \cdot K_{7y} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.14 \times 1.10 \times 7.50$	9.37 N/mm <sup>2</sup>
$\sigma_{c,adm} = K_2 \cdot K_3 \cdot K_8 \cdot \sigma_c$	$1.00 \times 1.00 \times 1.10 \times 7.90$	8.69 N/mm <sup>2</sup>
$\sigma_{c,L,adm} = K_2 \cdot K_3 \cdot K_4 \cdot K_8 \cdot \sigma_{c,L}$	$1.00 \times 1.00 \times 1.14 \times 1.10 \times 2.40$	3.01 N/mm <sup>2</sup>
$T_{adm} = K_2 \cdot K_3 \cdot K_8 \cdot T$	$1.00 \times 1.00 \times 1.10 \times 0.71$	0.78 N/mm <sup>2</sup>
$E = K_2 \cdot K_20 \cdot E_{mean}$ (Compression)	$1.00 \times 1.00 \times 10800$	8208.0 N/mm <sup>2</sup>
$E = K_2 \cdot E_{mean}$ (Deflection)	$1.00 \times 10800$	10800.0 N/mm <sup>2</sup>

#### Compression Resistance

$\lambda = \text{Max}(L_{ex}/r_x, L_{ey}/r_y)$	$\text{Max}(335/5.774, 335/2.714) \leq 180$	123.5	OK
$K_{12} = \text{fn}(\lambda, K_3, \sigma_c, E)$	123.53, 7.90, 8208	0.319	
$\sigma_{c,adm} = K_{12} \cdot \sigma_{c,adm}$	$0.319 \times 8.69$	2.77 N/mm <sup>2</sup>	
$\sigma_{c,a} = F/\text{Area}$	$1.956 / 188 \leq 2.77$	0.10 N/mm <sup>2</sup>	OK

#### Axial Load with Moments Check

Critical Design Location	X = 3.352		
$\sigma_{mx,a} = M_x/Z_x$	$0.520 / 626.67 \leq 8.63$	0.83 N/mm <sup>2</sup>	OK
$\sigma_{my,a} = M_y/Z_y$	$0.011 / 294.53 \leq 9.37$	0.04 N/mm <sup>2</sup>	OK
$\sigma_{mx,adm} = \sigma_{mx,adm} (1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$8.63 (1 - 1.5 \times 0.319 \times 0.10 / 5.31)$	8.55 N/mm <sup>2</sup>	
$\sigma_{my,adm} = \sigma_{my,adm} (1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$9.37 (1 - 1.5 \times 0.319 \times 0.10 / 5.31)$	9.29 N/mm <sup>2</sup>	
$\sigma_c / \sigma_{c,adm} + \sigma_{mx} / \sigma_{mx,adm} + \sigma_{my} / \sigma_{my,adm}$	$0.10 / 2.77 + 0.83 / 8.55 + 0.04 / 9.29$	0.139	OK

#### Shear and Bearing Check

Critical Design Location	X = 2.807		
$T_a = 1.5 \sqrt{(F_{vx}^2 + F_{vy}^2)} / \text{Area}$	$1.5 \sqrt{(0.317^2 + 0.006^2)} / 188 \leq 0.78$	0.03 N/mm <sup>2</sup>	OK
$\sigma_{c,Lax} = F_{vx} / (b \cdot B_x)$	$0.317 / (94 \times 75) \leq 3.01$	0.04 N/mm <sup>2</sup>	OK
$\sigma_{c,Lay} = F_{vy} / (h \cdot B_y)$	$0.006 / (200 \times 75) \leq 3.01$	0.00 N/mm <sup>2</sup>	OK

#### Deflection Check (Shear Deflection NOT Included)

Critical Load Case 002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)			
$\delta = \delta_m$	In-span $0.23 \leq L/333$	0.23 mm	OK

# WD Eng

Job No.	2466	Sheet No.	51	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Job Title.	47a Market Jew Street, Penzance						
Member.	Proposed room in the extension						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

## MASTERKEY : TIMBER DESIGN

### AXIAL LOAD WITH MOMENT DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 15 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 94, h = 200, 200x94 in Strength Class C24
Section Properties (c,cm <sup>3</sup> ,cm)	Area 188, Zx 626.7, Zy 294.5, rx 5.77, ry 2.71
Specification	1 : Internal use in continuously heated building Long term loading, 2 pieces of softwood, Load sharing
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Member Details	F = 0.229 kN, L = 3.749 m, Lx = 3.749 m, Ly = 3.749 m, Lex = 1.0 Lx, Ley = 1.0 Ly Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{mx,adm} = K_2 \cdot K_3 \cdot K_{7x} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.05 \times 1.10 \times 7.50$	8.63 N/mm <sup>2</sup>
$\sigma_{my,adm} = K_2 \cdot K_3 \cdot K_{7y} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.14 \times 1.10 \times 7.50$	9.37 N/mm <sup>2</sup>
$\sigma_{c,adm} = K_2 \cdot K_3 \cdot K_8 \cdot \sigma_c$	$1.00 \times 1.00 \times 1.10 \times 7.90$	8.69 N/mm <sup>2</sup>
$\sigma_{c,L,adm} = K_2 \cdot K_3 \cdot K_4 \cdot K_8 \cdot \sigma_{c,L}$	$1.00 \times 1.00 \times 1.14 \times 1.10 \times 1.90$	2.38 N/mm <sup>2</sup>
$T_{adm} = K_2 \cdot K_3 \cdot K_8 \cdot T$	$1.00 \times 1.00 \times 1.10 \times 0.71$	0.78 N/mm <sup>2</sup>
$E = K_2 \cdot K_20 \cdot E_{mean}$ (Compression)	$1.00 \times 1.00 \times 10800$	8208.0 N/mm <sup>2</sup>
$E = K_2 \cdot E_{mean}$ (Deflection)	$1.00 \times 10800$	10800.0 N/mm <sup>2</sup>

#### Compression Resistance

$\lambda = \text{Max}(L_{ex}/r_x, L_{ey}/r_y)$	$\text{Max}(375/5.774, 375/2.714) \leq 180$	138.2	OK
$K_{12} = \text{fn}(\lambda, K_3, \sigma_c, E)$	138.16, 7.90, 8208	0.268	
$\sigma_{c,adm} = K_{12} \cdot \sigma_{c,adm}$	$0.268 \times 8.69$	2.33 N/mm <sup>2</sup>	
$\sigma_{c,a} = F/\text{Area}$	$0.229 / 188 \leq 2.33$	0.01 N/mm <sup>2</sup>	OK

#### Axial Load with Moments Check

Critical Design Location	X = 3.749		
$\sigma_{mx,a} = M_x/Z_x$	$0.630 / 626.67 \leq 8.63$	1.01 N/mm <sup>2</sup>	OK
$\sigma_{my,a} = M_y/Z_y$	$0.030 / 294.53 \leq 9.37$	0.10 N/mm <sup>2</sup>	OK
$\sigma_{mx,adm} = \sigma_{mx,adm}(1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$8.63 (1 - 1.5 \times 0.268 \times 0.01 / 4.24)$	8.62 N/mm <sup>2</sup>	
$\sigma_{my,adm} = \sigma_{my,adm}(1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$9.37 (1 - 1.5 \times 0.268 \times 0.01 / 4.24)$	9.36 N/mm <sup>2</sup>	
$\sigma_c / \sigma_{c,adm} + \sigma_{mx} / \sigma_{mx,adm} + \sigma_{my} / \sigma_{my,adm}$	$0.01 / 2.33 + 1.01 / 8.62 + 0.10 / 9.36$	0.133	OK

#### Shear and Bearing Check

Critical Design Location	X = 2.953		
$T_a = 1.5 \sqrt{(F_{vx}^2 + F_{vy}^2)} / \text{Area}$	$1.5 \sqrt{(0.32^2 + 0.009^2)} / 188 \leq 0.78$	0.03 N/mm <sup>2</sup>	OK
$\sigma_{c,Lax} = F_{vx} / (b \cdot B_x)$	$0.32 / (94 \times 75) \leq 2.38$	0.05 N/mm <sup>2</sup>	OK
$\sigma_{c,Lay} = F_{vy} / (h \cdot B_y)$	$0.009 / (200 \times 75) \leq 2.38$	0.00 N/mm <sup>2</sup>	OK

#### Deflection Check (Shear Deflection NOT Included)

Critical Load Case 002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)			
$\delta = \delta_m$	In-span $0.37 \leq L/333$	0.37 mm	OK

# WD Eng

Job No.	2466	Sheet No.	52	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

## MASTERKEY : TIMBER DESIGN

### AXIAL LOAD WITH MOMENT DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 7 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 94, h = 200, 200x94 in Strength Class C24, No wane at bearing
Section Properties (c,cm <sup>3</sup> ,cm)	Area 188, Zx 626.7, Zy 294.5, rx 5.77, ry 2.71
Specification	1 : Internal use in continuously heated building Long term loading, 2 pieces of softwood
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Member Details	F = -1.925 kN, L = 0.601 m, Lx = 0.601 m, Ly = 0.601 m, Lex = 1.0 Lx, Ley = 1.0 Ly Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{mx,adm} = K_2 \cdot K_3 \cdot K_{7x} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.05 \times 1.00 \times 7.50$	7.84 N/mm <sup>2</sup>
$\sigma_{my,adm} = K_2 \cdot K_3 \cdot K_{7y} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.14 \times 1.00 \times 7.50$	8.52 N/mm <sup>2</sup>
$\sigma_{t,adm} = K_2 \cdot K_3 \cdot K_8 \cdot K_{14} \cdot \sigma_t$	$1.00 \times 1.00 \times 1.00 \times 1.05 \times 4.50$	4.71 N/mm <sup>2</sup>
$\sigma_{c\perp,adm} = K_2 \cdot K_3 \cdot K_4 \cdot K_8 \cdot \sigma_{c\perp}$	$1.00 \times 1.00 \times 1.14 \times 1.00 \times 2.40$	2.74 N/mm <sup>2</sup>
$T_{adm} = K_2 \cdot K_3 \cdot K_8 \cdot T$	$1.00 \times 1.00 \times 1.00 \times 0.71$	0.71 N/mm <sup>2</sup>
$E = K_2 \cdot E_{mean}$	$1.00 \times 10800$	10800.0 N/mm <sup>2</sup>

#### Tensile Resistance

$\sigma_{t,a} = F/Area$	$1.925 / 188 \leq 4.71$	0.10 N/mm <sup>2</sup>	OK
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#### Axial Load with Moments Check

Critical Design Location	X = 0.601		
$\sigma_{mx,a} = Mx/Zx$	$0.728 / 626.67 \leq 7.84$	1.16 N/mm <sup>2</sup>	OK
$\sigma_{my,a} = My/Zy$	$0.297 / 294.53 \leq 8.52$	1.01 N/mm <sup>2</sup>	OK
$\sigma_t / \sigma_{t,adm} + \sigma_{mx} / \sigma_{mx,adm} + \sigma_{my} / \sigma_{my,adm}$	$0.10 / 4.71 + 1.16 / 7.84 + 1.01 / 8.52$	0.288	OK

#### Shear and Bearing Check

Critical Design Location	X = 0.570		
$T_a = 1.5 \sqrt{(Fvx^2 + Fvy^2)} / Area$	$1.5 \sqrt{(1.713^2 + 0.65^2)} / 188 \leq 0.71$	0.15 N/mm <sup>2</sup>	OK
$\sigma_{c\perp,ax} = Fvx / (b \cdot Bx)$	$1.713 / (94 \times 75) \leq 2.74$	0.24 N/mm <sup>2</sup>	OK
$\sigma_{c\perp,ay} = Fvy / (h \cdot By)$	$0.65 / (200 \times 75) \leq 2.74$	0.04 N/mm <sup>2</sup>	OK

#### Deflection Check (Shear Deflection NOT Included)

Critical Load Case 002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)			
$\delta = \delta_m$	In-span $0.04 \leq L/333$	0.04 mm	OK

# WD Eng

Job No.	2466	Sheet No.	53	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Job Title.	47a Market Jew Street, Penzance						
Member.	Proposed room in the extension						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

## MASTERKEY : TIMBER DESIGN

### AXIAL LOAD WITH MOMENT DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 8 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 94, h = 200, 200x94 in Strength Class C24, No wane at bearing
Section Properties (c,cm <sup>3</sup> ,cm)	Area 188, Zx 626.7, Zy 294.5, rx 5.77, ry 2.71
Specification	1 : Internal use in continuously heated building Long term loading, 2 pieces of softwood, Load sharing
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Member Details	F = 1.96 kN, L = 3.481 m, Lx = 3.481 m, Ly = 3.481 m, Lex = 1.0 Lx, Ley = 1.0 Ly Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{mx,adm} = K_2 \cdot K_3 \cdot K_{7x} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.05 \times 1.10 \times 7.50$	8.63 N/mm <sup>2</sup>
$\sigma_{my,adm} = K_2 \cdot K_3 \cdot K_{7y} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.14 \times 1.10 \times 7.50$	9.37 N/mm <sup>2</sup>
$\sigma_{c,adm} = K_2 \cdot K_3 \cdot K_8 \cdot \sigma_c$	$1.00 \times 1.00 \times 1.10 \times 7.90$	8.69 N/mm <sup>2</sup>
$\sigma_{c,L,adm} = K_2 \cdot K_3 \cdot K_4 \cdot K_8 \cdot \sigma_{c,L}$	$1.00 \times 1.00 \times 1.14 \times 1.10 \times 2.40$	3.01 N/mm <sup>2</sup>
$T_{adm} = K_2 \cdot K_3 \cdot K_8 \cdot T$	$1.00 \times 1.00 \times 1.10 \times 0.71$	0.78 N/mm <sup>2</sup>
$E = K_2 \cdot K_{20} \cdot E_{mean}$ (Compression)	$1.00 \times 1.00 \times 10800$	8208.0 N/mm <sup>2</sup>
$E = K_2 \cdot E_{mean}$ (Deflection)	$1.00 \times 10800$	10800.0 N/mm <sup>2</sup>

#### Compression Resistance

$\lambda = \text{Max}(L_{ex}/r_x, L_{ey}/r_y)$	$\text{Max}(348/5.774, 348/2.714) \leq 180$	128.3	OK
$K_{12} = \text{fn}(\lambda, K_3, \sigma_c, E)$	128.28, 7.90, 8208	0.301	
$\sigma_{c,adm} = K_{12} \cdot \sigma_{c,adm}$	$0.301 \times 8.69$	2.61 N/mm <sup>2</sup>	
$\sigma_{c,a} = F/\text{Area}$	$1.96 / 188 \leq 2.61$	0.10 N/mm <sup>2</sup>	OK

#### Axial Load with Moments Check

Critical Design Location	X = 1.958		
$\sigma_{mx,a} = M_x/Z_x$	$0.718 / 626.67 \leq 8.63$	1.15 N/mm <sup>2</sup>	OK
$\sigma_{my,a} = M_y/Z_y$	$0.023 / 294.53 \leq 9.37$	0.08 N/mm <sup>2</sup>	OK
$\sigma_{mx,adm} = \sigma_{mx,adm}(1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$8.63 (1 - 1.5 \times 0.301 \times 0.10 / 4.92)$	8.54 N/mm <sup>2</sup>	
$\sigma_{my,adm} = \sigma_{my,adm}(1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$9.37 (1 - 1.5 \times 0.301 \times 0.10 / 4.92)$	9.28 N/mm <sup>2</sup>	
$\sigma_c / \sigma_{c,adm} + \sigma_{mx} / \sigma_{mx,adm} + \sigma_{my} / \sigma_{my,adm}$	$0.10 / 2.61 + 1.15 / 8.54 + 0.08 / 9.28$	0.183	OK

#### Shear and Bearing Check

Critical Design Location	X = 0.000		
$T_a = 1.5 \sqrt{(F_{vx}^2 + F_{vy}^2)} / \text{Area}$	$1.5 \sqrt{(1.141^2 + 0.034^2)} / 188 \leq 0.78$	0.09 N/mm <sup>2</sup>	OK
$\sigma_{c,Lax} = F_{vx} / (b \cdot B_x)$	$1.141 / (94 \times 75) \leq 3.01$	0.16 N/mm <sup>2</sup>	OK
$\sigma_{c,Lay} = F_{vy} / (h \cdot B_y)$	$0.034 / (200 \times 75) \leq 3.01$	0.00 N/mm <sup>2</sup>	OK

#### Deflection Check (Shear Deflection NOT Included)

Critical Load Case 002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)			
$\delta = \delta_m$	In-span $1.23 \leq L/333$	1.23 mm	OK

# WD Eng

Job No.	2466	Sheet No.	54	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Job Title.	47a Market Jew Street, Penzance						
Member.	Proposed room in the extension						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

## MASTERKEY : TIMBER DESIGN

### AXIAL LOAD WITH MOMENT DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 9 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 94, h = 200, 200x94 in Strength Class C24, No wane at bearing
Section Properties (c,cm <sup>3</sup> ,cm)	Area 188, Zx 626.7, Zy 294.5, rx 5.77, ry 2.71
Specification	1 : Internal use in continuously heated building Long term loading, 2 pieces of softwood
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Member Details	F = 0.858 kN, L = 4.995 m, Lx = 4.995 m, Ly = 4.995 m, Lex = 1.0 Lx, Ley = 1.0 Ly Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{mx,adm} = K_2 \cdot K_3 \cdot K_{7x} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.05 \times 1.00 \times 7.50$	7.84 N/mm <sup>2</sup>
$\sigma_{my,adm} = K_2 \cdot K_3 \cdot K_{7y} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.14 \times 1.00 \times 7.50$	8.52 N/mm <sup>2</sup>
$\sigma_{c,adm} = K_2 \cdot K_3 \cdot K_8 \cdot \sigma_c$	$1.00 \times 1.00 \times 1.00 \times 7.90$	7.90 N/mm <sup>2</sup>
$\sigma_{c,L,adm} = K_2 \cdot K_3 \cdot K_4 \cdot K_8 \cdot \sigma_{c,L}$	$1.00 \times 1.00 \times 1.14 \times 1.00 \times 2.40$	2.74 N/mm <sup>2</sup>
$T_{adm} = K_2 \cdot K_3 \cdot K_8 \cdot T$	$1.00 \times 1.00 \times 1.00 \times 0.71$	0.71 N/mm <sup>2</sup>
$E = K_2 \cdot K_{20} \cdot E_{mean}$ (Compression)	$1.00 \times 1.00 \times 10800$	8208.0 N/mm <sup>2</sup>
$E = K_2 \cdot E_{mean}$ (Deflection)	$1.00 \times 10800$	10800.0 N/mm <sup>2</sup>

#### Compression Resistance

$\lambda = \text{Max}(L_{ex}/r_x, L_{ey}/r_y)$	$\text{Max}(500/5.774, 500/2.714) \leq 180$	184.1	Warning
$K_{12} = \text{fn}(\lambda, K_3, \sigma_c, E)$	184.08, 7.90, 8208	0.165	
$\sigma_{c,adm} = K_{12} \cdot \sigma_{c,adm}$	$0.165 \times 7.90$	1.30 N/mm <sup>2</sup>	
$\sigma_{c,a} = F/\text{Area}$	$0.858 / 188 \leq 1.30$	0.05 N/mm <sup>2</sup>	OK

#### Axial Load with Moments Check

Critical Design Location	X = 0.000		
$\sigma_{mx,a} = M_x/Z_x$	$1.819 / 626.67 \leq 7.84$	2.90 N/mm <sup>2</sup>	OK
$\sigma_{my,a} = M_y/Z_y$	$0.476 / 294.53 \leq 8.52$	1.62 N/mm <sup>2</sup>	OK
$\sigma_{mx,adm} = \sigma_{mx,adm}(1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$7.84 (1 - 1.5 \times 0.165 \times 0.05 / 2.39)$	7.81 N/mm <sup>2</sup>	
$\sigma_{my,adm} = \sigma_{my,adm}(1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$8.52 (1 - 1.5 \times 0.165 \times 0.05 / 2.39)$	8.48 N/mm <sup>2</sup>	
$\sigma_c / \sigma_{c,adm} + \sigma_{mx} / \sigma_{mx,adm} + \sigma_{my} / \sigma_{my,adm}$	$0.05 / 1.30 + 2.90 / 7.81 + 1.62 / 8.48$	0.598	OK

#### Shear and Bearing Check

Critical Design Location	X = 0.000		
$T_a = 1.5 \sqrt{(F_{vx}^2 + F_{vy}^2)} / \text{Area}$	$1.5 \sqrt{(2.68^2 + 0.517^2)} / 188 \leq 0.71$	0.22 N/mm <sup>2</sup>	OK
$\sigma_{c,Lax} = F_{vx} / (b \cdot B_x)$	$2.68 / (94 \times 75) \leq 2.74$	0.38 N/mm <sup>2</sup>	OK
$\sigma_{c,Lay} = F_{vy} / (h \cdot B_y)$	$0.517 / (200 \times 75) \leq 2.74$	0.03 N/mm <sup>2</sup>	OK

#### Deflection Check (Shear Deflection NOT Included)

Critical Load Case 002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)			
$\delta = \delta_m$	In-span $1.56 \leq L/333$	1.56 mm	OK



Job No.	2466	Sheet No.	55	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Job Title.	47a Market Jew Street, Penzance				
Member.	Proposed room in the extension				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

## MASTERKEY : TIMBER DESIGN

### AXIAL LOAD WITH MOMENT DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 10 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 94, h = 200, 200x94 in Strength Class C24, No wane at bearing
Section Properties (c,cm <sup>3</sup> ,cm)	Area 188, Zx 626.7, Zy 294.5, rx 5.77, ry 2.71
Specification	1 : Internal use in continuously heated building Long term loading, 2 pieces of softwood
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Member Details	F = 0.592 kN, L = 3.458 m, Lx = 3.458 m, Ly = 3.458 m, Lex = 1.0 Lx, Ley = 1.0 Ly Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{mx,adm} = K_2 \cdot K_3 \cdot K_{7x} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.05 \times 1.00 \times 7.50$	7.84 N/mm <sup>2</sup>
$\sigma_{my,adm} = K_2 \cdot K_3 \cdot K_{7y} \cdot K_8 \cdot \sigma_m$	$1.00 \times 1.00 \times 1.14 \times 1.00 \times 7.50$	8.52 N/mm <sup>2</sup>
$\sigma_{c,adm} = K_2 \cdot K_3 \cdot K_8 \cdot \sigma_c$	$1.00 \times 1.00 \times 1.00 \times 7.90$	7.90 N/mm <sup>2</sup>
$\sigma_{c,L,adm} = K_2 \cdot K_3 \cdot K_4 \cdot K_8 \cdot \sigma_{c,L}$	$1.00 \times 1.00 \times 1.14 \times 1.00 \times 2.40$	2.74 N/mm <sup>2</sup>
$T_{adm} = K_2 \cdot K_3 \cdot K_8 \cdot T$	$1.00 \times 1.00 \times 1.00 \times 0.71$	0.71 N/mm <sup>2</sup>
$E = K_2 \cdot K_20 \cdot E_{mean}$ (Compression)	$1.00 \times 1.00 \times 10800$	8208.0 N/mm <sup>2</sup>
$E = K_2 \cdot E_{mean}$ (Deflection)	$1.00 \times 10800$	10800.0 N/mm <sup>2</sup>

#### Compression Resistance

$\lambda = \text{Max}(L_{ex}/r_x, L_{ey}/r_y)$	$\text{Max}(346/5.774, 346/2.714) \leq 180$	127.4	OK
$K_{12} = \text{fn}(\lambda, K_3, \sigma_c, E)$	127.43, 7.90, 8208	0.304	
$\sigma_{c,adm} = K_{12} \cdot \sigma_{c,adm}$	$0.304 \times 7.90$	2.40 N/mm <sup>2</sup>	
$\sigma_{c,a} = F/\text{Area}$	$0.592 / 188 \leq 2.40$	0.03 N/mm <sup>2</sup>	OK

#### Axial Load with Moments Check

Critical Design Location	$X = 2.032$		
$\sigma_{mx,a} = M_x/Z_x$	$0.789 / 626.67 \leq 7.84$	1.26 N/mm <sup>2</sup>	OK
$\sigma_{my,a} = M_y/Z_y$	$0.006 / 294.53 \leq 8.52$	0.02 N/mm <sup>2</sup>	OK
$\sigma_{mx,adm} = \sigma_{mx,adm} (1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$7.84 (1 - 1.5 \times 0.304 \times 0.03 / 4.99)$	7.82 N/mm <sup>2</sup>	
$\sigma_{my,adm} = \sigma_{my,adm} (1 - 1.5 K_{12} \cdot \sigma_{c,a} / \sigma_e)$	$8.52 (1 - 1.5 \times 0.304 \times 0.03 / 4.99)$	8.50 N/mm <sup>2</sup>	
$\sigma_c / \sigma_{c,adm} + \sigma_{mx} / \sigma_{mx,adm} + \sigma_{my} / \sigma_{my,adm}$	$0.03 / 2.40 + 1.26 / 7.82 + 0.02 / 8.50$	0.177	OK

#### Shear and Bearing Check

Critical Design Location	$X = 0.000$		
$T_a = 1.5 \sqrt{(F_{vx}^2 + F_{vy}^2)} / \text{Area}$	$1.5 \sqrt{(1.142^2 + 0.004^2)} / 188 \leq 0.71$	0.09 N/mm <sup>2</sup>	OK
$\sigma_{c,Lax} = F_{vx} / (b \cdot B_x)$	$1.142 / (94 \times 75) \leq 2.74$	0.16 N/mm <sup>2</sup>	OK
$\sigma_{c,Lay} = F_{vy} / (h \cdot B_y)$	$0.004 / (200 \times 75) \leq 2.74$	0.00 N/mm <sup>2</sup>	OK

#### Deflection Check (Shear Deflection NOT Included)

Critical Load Case 002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)			
$\delta = \delta_m$	In-span $1.30 \leq L/333$	1.30 mm	OK



# WD Eng

Job No.	2466	Sheet No.	56	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

## MASTERKEY : TIMBER DESIGN

### AXIAL LOAD WITH MOMENT DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 18 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 47, h = 200, 200x47 in Strength Class C24, No wane at bearing
Section Properties (c,cm <sup>3</sup> ,cm)	Area 94, Zx 313.3, Zy 73.6, rx 5.77, ry 1.36
Specification	1 : Internal use in continuously heated building Long term loading
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Member Details	F = 0.0 kN, L = 2.96 m, Lx = 2.96 m, Ly = 2.96 m, Lex = 1.0 Lx, Ley = 1.0 Ly Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{mx.adm} = K_2.K_3.K_7.K_8.\sigma_m$	$1.00 \times 1.00 \times 1.05 \times 1.00 \times 7.50$	7.84 N/mm <sup>2</sup>
$\sigma_{my.adm} = K_2.K_3.K_7.K_8.\sigma_m$	$1.00 \times 1.00 \times 1.17 \times 1.00 \times 7.50$	8.78 N/mm <sup>2</sup>
$\sigma_{c\perp.adm} = K_2.K_3.K_4.K_8.\sigma_{c\perp}$	$1.00 \times 1.00 \times 1.14 \times 1.00 \times 2.40$	2.74 N/mm <sup>2</sup>
$T_{adm} = K_2.K_3.K_8.T$	$1.00 \times 1.00 \times 1.00 \times 0.71$	0.71 N/mm <sup>2</sup>
$E = K_2.E_{mean}$	$1.00 \times 10800$	10800.0 N/mm <sup>2</sup>

#### Axial Load with Moments Check

Critical Design Location	X = 0.000		
$\sigma_{mx.a} = Mx/Zx$	$2.008 / 313.33 \leq 7.84$	6.41 N/mm <sup>2</sup>	OK
$\sigma_{mx}/\sigma_{mx.adm}$	$6.41/7.84$	0.817	OK

#### Shear and Bearing Check

Critical Design Location	X = 0.000		
$T_a = 1.5 F_v / \text{Area}$	$1.5 \times 3.671 / 94 \leq 0.71$	0.59 N/mm <sup>2</sup>	OK
$\sigma_{c\perp.ax} = F_vx / (b.Bx)$	$3.671 / (47 \times 75) \leq 2.74$	1.04 N/mm <sup>2</sup>	OK

#### Deflection Check (Shear Deflection NOT Included)

Critical Load Case 002 : Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)			
$\delta = \delta_m$	In-span $2.99 \leq L/333$	2.99 mm	OK

Job No.	2466	Sheet No.	57	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Job Title.	47a Market Jew Street, Penzance				
Member.	Proposed room in the extension				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

## MASTERKEY : TIMBER DESIGN

### FLITCH BEAM DESIGN TO BS 5268 : PART 2

#### Member TBL1Id 21 @ Level 1

#### Summary Design Data

Design Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Deflection Cases Covered	2, 7-8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38 & 40
Section Size	b = 47, h = 200, (2) 47 x 200 in Strength Class C24, no wane at bearing
Steel Plates Section Size	b = 10, h = 200, (1) 10 x 200 in Grade S 275
Section Properties (cm <sup>2</sup> , cm <sup>3</sup> , cm)	Area 94, Z <sub>x</sub> 1892.1, Z <sub>y</sub> 366.3, r <sub>x</sub> 5.77, r <sub>y</sub> 1.83
Steel Properties (cm <sup>2</sup> , cm <sup>4</sup> )	Area 20, I <sub>x</sub> 12654.3, I <sub>y</sub> 31.6
Specification	1 : Internal use in continuously heated building Long Term loading, 2 pieces of softwood
Integrated Design Critical Case	: Dead+Live 1.00D0+1.00D1+1.00L1 (Serviceability)
Steel Design Factor, $\gamma_{ult}$	All steel design forces factored by the user defined Ult/Serv factor of 1.2
Member Details	F = 0.303 kN, L = 4.375 m, L <sub>x</sub> = 4.375 m, L <sub>y</sub> = 4.375 m, L <sub>ex</sub> = 1.0 L <sub>x</sub> , L <sub>ey</sub> = 1.0 L <sub>y</sub> Bearing length B 75, Distance to Bearing 150 mm

#### Grade and Admissible Stresses (Strength Class C24)

$\sigma_{m,adm} = K_2 \cdot K_3 \cdot K_7 \cdot K_8 \cdot \sigma_m$	1.00 x 1.00 x 1.05 x 1.00 x 7.50	7.84 N/mm <sup>2</sup>
$\sigma_{c,adm} = K_2 \cdot K_3 \cdot K_8 \cdot \sigma_c$	1.00 x 1.00 x 1.00 x 7.90	7.90 N/mm <sup>2</sup>
$\sigma_{c\perp,adm} = K_2 \cdot K_3 \cdot K_4 \cdot K_8 \cdot \sigma_{c\perp}$	1.00 x 1.00 x 1.14 x 1.00 x 2.40	2.74 N/mm <sup>2</sup>
$T_{adm} = K_2 \cdot K_3 \cdot K_8 \cdot T$	1.00 x 1.00 x 1.00 x 0.71	0.71 N/mm <sup>2</sup>
$E = K_2 \cdot K_2 \cdot E_{m,mean}$ (Compression)	1.00 x 1.00 x 10800	8208.0 N/mm <sup>2</sup>
$E = K_2 \cdot E_{m,mean}$ (Deflection)	1.00 x 10800	10800.0 N/mm <sup>2</sup>

#### Compression Resistance

$\lambda = \text{Max}(L_{ex} / r_x, L_{ey} / r_y)$	Max(4375 / 57.74, 4375 / 18.32) = 250	238.83	OK
$K_{12} = \text{fn}(\lambda, \sigma_c, E)$	238.83, 7.9, 7632	0.092	
$\sigma_{c,adm} = K_{12} \cdot \sigma_{c,adm}$	0.092 x 7.9	0.73 N/mm <sup>2</sup>	
$\sigma_{c,a} = F / \text{Area}$	0.303 / 188 = 0.73	0.016 N/mm <sup>2</sup>	OK

#### Bending Stresses in Timber

$\sigma_{t,x} = M_x / Z_t$	9.78 / 1892.1 = 7.84	5.17 N/mm <sup>2</sup>	OK
$\sigma_{t,y} = M_y / Z_t$	0.001 / 366.3 = 8.78	0.003 N/mm <sup>2</sup>	OK
$\sigma_{mx,adm} \cdot (1 - 1.5 \cdot K_{12} \cdot \sigma_{c,a} / \sigma_e)$	7.84 x (1 - 1.5 x 0.092 x 0.016) / 1.25	7.83 N/mm <sup>2</sup>	
$\sigma_{my,adm} \cdot (1 - 1.5 \cdot K_{12} \cdot \sigma_{c,a} / \sigma_e)$	8.78 x (1 - 1.5 x 0.092 x 0.016) / 1.25	8.76 N/mm <sup>2</sup>	
$U_{comb} = U_c + U_{mt,x} + U_{mt,y}$	0.016/0.73 + 5.17/7.83 + 0.003/8.76	0.683	OK

#### Bending Stresses in Steel

$\sigma_{s,x} = \gamma_{ult} \cdot m_r \cdot M_x / Z_s$	(1.2 x 18.98 x 9.78) / 1892.09 = 275	117.72 N/mm <sup>2</sup>	OK
$\sigma_{s,y} = \gamma_{ult} \cdot m_r \cdot M_y / Z_s$	(1.2 x 18.98 x 0.001) / 3809.49 = 275	0.006 N/mm <sup>2</sup>	OK
$U_{comb} = U_{ms,x} + U_{ms,y}$	0.428 + 0	0.428	OK

#### Shear and Bearing Check

$T_{a,x} = \sqrt{(f_{vx} \cdot F_{Vx} / A_t)^2 + (f_{vy} \cdot F_{Vy} / A_t)^2}$	$\sqrt{(0.497 \times 9.92^2 + 1.32 \times 0.019^2)}$	0.262 N/mm <sup>2</sup>	OK
$\sigma_{ca} = F_v / (b \cdot B \cdot N_o t)$	9.92 / (47 x 75 x 2) = 2.74	1.41 N/mm <sup>2</sup>	OK
$\sigma_{ca} = F_v / (b \cdot B \cdot N_o t)$	0.019 / (200 x 10) = 2.4	0.01 N/mm <sup>2</sup>	OK

#### Deflection

9.39 = L / 333		9.39 mm	OK
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#### Minimum Bolt Capacity

Basic Data	dia = 12 mm, baspar = 3.12 kN, K <sub>46</sub> = 1.25, K <sub>56</sub> = 1, K <sub>57</sub> = 1	
Permissible Shear & Bearing Stress	pbss = 160 N/mm <sup>2</sup> , pbbs = 460 N/mm <sup>2</sup>	
Load for bolt from Annex G BS 5268-2		
$P_{bit,90} = \text{baspar} \cdot K_{46} \cdot K_{56} \cdot K_{57}$	Perpendicular to grain, 3.12 x 1.25 x 1 x 1	4.15 kN
$P_{bit,0} = \text{baspar} \cdot K_{46} \cdot K_{56} \cdot K_{57}$	Parallel to grain, 4.44 x 1.25 x 1 x 1	5.54 kN
Bearing, $P_{bb} = d \cdot t_p \cdot p_{bb}$	(12 x 10 x 460) / 1000	55.2 kN
Shear, $P_s = p_s \cdot A_s$	(160 x 84) / 1000	13.44 kN
Bearing, $P_{bs} = k_{bs} \cdot d \cdot t_p \cdot p_{bs}$	1 x 12 x 10 x 410	49.2 kN

# WDCEng

Job No.	2466	Sheet No.	58	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

Check  $P_{bs} < 0.5 \cdot k_{bs} \cdot e \cdot t_p \cdot p_{bs}$   $49.2 < 0.5 \times 1 \times 55 \times 10 \times 410$  112.75 OK  
Bolt Capacity =  $\min(2 \times 4.15, 2 \times 13.44, 1 \times 55.2)$  4.15 kN  
 $\min(N_{pin}, P_{bit}, N_{pin}, P_s, N_{pit}, P_{bs})$

### Minimum Number Of Bolts Along Length

$P_{stl,x} = UDL \cdot L \cdot I_{eff,s} / I_{cmb}$   $5.29 \times 4.38 \times 12.7e3 / 18.9e3$  15.47 kN  
 $P_{stl,y} = \gamma_{ult} \cdot F_v \cdot A_{eff,s} \cdot \gamma_s / I_{cmb,y} \cdot L$   $100 \times 0.023 \times 94 \times 2.85 / 1904.74 \times 4.38$  1.4 kN  
 $P_{stl,Total} = \text{Sqrt}(P_{stl,x}^2 / N_{pin}^2 + P_{stl,y}^2)$   $\text{Sqrt}(15.47^2 / 2^2 + 1.4^2)$  7.86 kN  
Max Bolt Spc. =  $\min(2.5 \cdot h_t, 600)$   $\min(2.5 \times 200, 600)$  500 mm  
 $N_{bmin} = L / \text{Max Spacing}$   $4375 / 500$  9  
No. Bolts =  $\max(N_{bmin}, P_{stl} / \text{Bolt}_{cap})$   $\max(9, 7.86 / 4.15)$  9  
Bolt load =  $P_{stl} / \text{Num Bolts}$   $7.86 / 9$  0.874 kN  
 $U_{bolt} = \text{Bolt Load} / \text{Bolt Capacity}$   $0.874 / 4.15$  0.211 OK

### Minimum Number Of Bolts At Ends

Proportion of load in steel plates  
 $P_{stl} = F_v \cdot I_{eff,s} / I_{cmb}$   $(11.9 \times 12.7e3 / 18.9e3)$  7.96 kN  
Num Bolts =  $\max(P_{stl} / P_{bolt}, 2)$   $\max(7.96 / 4.15, 2)$  2

### Minimum Bolt Spacing

Spacing =  $4 \cdot \text{dia}$   $4 \times 12$  48 mm

### Bolt Summary

Minimum requirement for supports: 2 No. 12 mm diameter Grade 4.6 bolts.  
Minimum requirement for beam: 9, 12 mm diameter Grade 4.6 bolts, placed at 500 mm centres, alternately staggered 50 mm above and below the centre line.

Job No.	2466	Sheet No.	59	Rev.	
Client.	Mr T Hudson				
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001				
Calc by.	BD	Date	5.12.2023	Chd by.	BD
		Date	11.12.2023		

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

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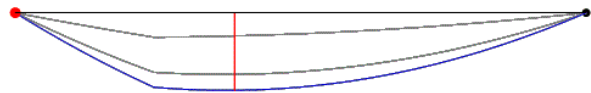
## AXIAL WITH MOMENTS (MEMBER)

### Member SBL1Id 1 @ Level 1 in Load Case 5

Member Loading and Member Forces

Loading Combination : 1 UT + 1.4 D0 + 1.4 D1 + 1.6 L1

D1 D 077.010 (kN/m<sup>3</sup>)  
 D1 UDLY -001.100 (kN/m)  
 L1 UDLY -003.200 (kN/m)  
 D1 PY -008.200 1.165 (kN,m)  
 L1 PY -004.100 1.165 (kN,m)



#### Member Forces in Load Case 5 and Maximum Deflection from Load Case 2

Member No.	Node End 1 End 2	Axial Force (kN)	Shear Force (kN)	Bending Moment (kNm)	Maximum Moment (kNm)	Maximum Deflection (mm @ m)
1	1	0.097C	30.473	0.000	32.049	10.532
	2	0.097C	-21.189	0.000	@ 1.763	@ 2.302

### Classification and Properties (BS 5950: 2000)

Section (25.09 kg/m) 203x133 UB 25 [S 275]  
 Class = Fn(b/T,d/t,py,F,Mx,My) 8.54, 30.25, 275, 0.1, 32.04, 0 (Axial: Non-Slender) Plastic  
 Auto Design Load Cases 1, 3-6, 9, 11, 13, 15, 17, 19, 21, 23, 25, 27, 29, 31, 33, 35, 37 & 39

### Shear Capacity Check

Fvx/Pvx 30.473 / 191.11 = 0.159 OK

### Local Capacity Check

Fvx/Pvx 0.501 / 191.11 = 0.003 Low Shear  
 Mcx = py.Sxx ≤ 1.2 py.Zxx 275 x 257.7 ≤ 1.2 x 275 x 230.42 = 70.868 kN.m  
 Pz = Ag.py 31.96 x 275 = 878.9 kN  
 n = F/Pz 0.097 / 878.9 = 0.000 OK  
 Srx = Fn(Sxx,) 257.7, 0 257.7 cm<sup>3</sup>  
 Mrx = Srx.py 257.7 x 275 70.868 kN.m  
 (Mx/Mrx)<sup>2</sup> + (My/Mry)<sup>2</sup> (32.028/70.868)<sup>2</sup> + (0)<sup>2</sup> = 0.204 OK

### Compression Resistance Pc

λx = Lex/rxx 100x1x4.8/8.56 = 56.1 OK  
 Pcx = Area.pcx 31.96x244.338/10 = 780.903 kN Table 24 a  
 λy = Ley/ryy 100x1x4.8/3.11 = 154.3 OK  
 Pcy = Area.pcy 31.96x70.8/10 = 226.267 kN Table 24 b

### Equivalent Uniform Moment Factors mLT, mx, my and myx

mLT = 0.2 + (.15M2 + .5M3 + .15M4)/Mmax 0.2 + (.15x31 + .5x31 + .15x20)/32 = 0.44 0.919 Table 18  
 my = 0.2 + (.1M2 + .6M3 + .1M4)/Mmax 0.2 + (.1x0 + .6x0 + .1x0)/0 = .8x0/0 1 Table 26  
 mx = 0.2 + (.1M2 + .6M3 + .1M4)/Mmax 0.2 + (.1x31 + .6x31 + .1x20)/32 = .8x32/32 0.934 Table 26  
 myx = 0.2 + (.1M2 + .6M3 + .1M4)/Mmax 0.2 + (.1x0 + .6x0 + .1x0)/0 = .8x0/0 1 Table 26

### Lateral Buckling Check Mb

Le = 1.00 L 1 x 4.8 = 4.8 m  
 λ = Le/ryy 4.8 / 3.11 154.34 OK  
 v = Fn(x,Le,ryy,λ) 25.404, 4.8, 3.11, 154.34 0.77 Table 19  
 λLT = u.v.λ.√βw 0.878 x 0.77 x 154.34 √1 104.32  
 pb = Fn(py,λLT) 275, 104.32 117.73 N/mm<sup>2</sup> Table 16

# WDcEng

Job No.	2466	Sheet No.	60	Rev.			
Client.	Mr T Hudson						
Drgs.	2466-WDCE-STR-MJSP-M2-S-0001						
Calc by.	BD	Date	5.12.2023	Chd by.	BD	Date	11.12.2023

Job Title. 47a Market Jew Street, Penzance

Member. Proposed room in the extension

$M_b = S_{xx}.p_b \leq M_c$	$257.7 \times 117.73 \leq 70.868 =$	30.338 kN.m	
<b>Simplified Approach</b>			
$p_y.Z_x$	275x230.42	63.366 kN.m	
$F/P_c + m_x.M_x/p_y.Z_x$	$0.097/226.267 + 0.934 \times 32/63.4$	0.473	OK
$F/P_c + m_{LT}.M_{LT}/M_b$	$0.097/226.267 + 0.919 \times 32/30.3$	0.970	OK
<b>More Exact Approach</b>			
$Max = M_{cx}/(1 + .5F/P_{cx})$	$70.9/(1 + .5 \times 0.1/780.9)$	70.863 kN.m	
$F/P_{cx} + m_x.M_x/Max$	$0.1/780.9 + 0.934 \times 32/70.9$	0.423	OK
$F/P_{cy} + m_{LT}.M_{LT}/M_b$	$0.1/226.3 + 0.919 \times 32/30.3$	0.970	OK
<b>Deflection Check - Load Case 2</b>			
In-span $\delta \leq \text{Span}/360$	$10.53 \leq 4800 / 360$	10.53 mm	OK

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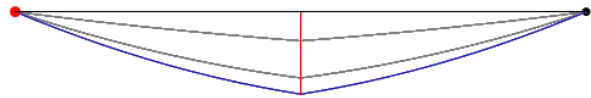
## AXIAL WITH MOMENTS (MEMBER)

### Member SBL1Id 2 @ Level 1 in Load Case 5

Member Loading and Member Forces

Loading Combination : 1 UT + 1.4 D0 + 1.4 D1 + 1.6 L1

D1 D 077.010 (kN/m<sup>3</sup>)  
 D1 UDLY -000.800 (kN/m)  
 L1 UDLY -002.400 (kN/m)  
 D1 PY -007.500 2.400 (kN,m)  
 L1 PY -003.200 2.400 (kN,m)



Member Forces in Load Case 5 and Maximum Deflection from Load Case 2

Member No.	Node End 1 End 2	Axial Force (kN)	Shear Force (kN)	Bending Moment (kNm)	Maximum Moment (kNm)	Maximum Deflection (mm @ m)
1	3	0.103C	20.541	0.000	34.021	10.099
	4	0.103C	-20.541	0.000	@ 2.400	@ 2.400

### Classification and Properties (BS 5950: 2000)

Section (25.09 kg/m) 203x133 UB 25 [S 275]  
 Class = Fn(b/T,d/t,py,F,Mx,My) 8.54, 30.25, 275, 0.1, 34.02, 0 (Axial: Non-Slender) Plastic  
 Auto Design Load Cases 1, 3-6, 9, 11, 13, 15, 17, 19, 21, 23, 25, 27, 29, 31, 33, 35, 37 & 39

### Shear Capacity Check

$F_vx/P_vx = 20.541 / 191.11 = 0.107$  OK

### Local Capacity Check

$F_vx/P_vx = 7.81 / 191.11 = 0.041$  Low Shear  
 $M_{cx} = p_y.S_{xx} \leq 1.2 p_y.Z_{xx} = 275 \times 257.7 \leq 1.2 \times 275 \times 230.42 = 70.868 \text{ kN.m}$   
 $P_z = A_g.p_y = 31.96 \times 275 = 878.9 \text{ kN}$   
 $n = F/P_z = 0.103 / 878.9 = 0.000$  OK  
 $S_{rx} = F_n(S_{xx},) = 257.7, 0 = 257.7 \text{ cm}^3$   
 $M_{rx} = S_{rx}.p_y = 257.7 \times 275 = 70.868 \text{ kN.m}$   
 $(M_x/M_{rx})^2 + (M_y/M_{ry})^2 = (34.021/70.868)^2 + (0)^2 = 0.23$  OK

### Compression Resistance Pc

$\lambda_x = L_{ex}/r_{xx} = 100 \times 1 \times 4.8 / 8.56 = 56.1$  OK  
 $P_{cx} = A_{area}.p_{cx} = 31.96 \times 244.338 / 10 = 780.903 \text{ kN}$  Table 24 a

### Lateral Buckling Check Mb

$M_b = M_c = \text{Fully Restrained} = 70.868 \text{ kN.m}$

### Simplified Approach

$p_y.Z_x = 275 \times 230.42 = 63.366 \text{ kN.m}$   
 $F/P_{cx} + m_x.M_x/p_y.Z_x = 0.103/780.903 + 0.922 \times 34/63.4 = 0.495$  OK  
 $F/P_{cy} + m_{LT}.M_{LT}/M_b = 0.103/878.9 + 0.884 \times 34/70.9 = 0.424$  OK

### More Exact Approach

$M_{ax} = M_{cx} / (1 + 5F/P_{cx}) = 70.9 / (1 + 5 \times 0.1 / 780.9) = 70.863 \text{ kN.m}$   
 $F/P_{cx} + m_x.M_x/M_{ax} = 0.1/780.9 + 0.922 \times 34/70.9 = 0.443$  OK  
 $F/P_{cy} + m_{LT}.M_{LT}/M_b = 0.1/878.9 + 0.884 \times 34/70.9 = 0.424$  OK

### Deflection Check - Load Case 2

In-span  $\delta \leq \text{Span}/360 = 10.1 \leq 4800 / 360 = 10.1 \text{ mm}$  OK

# WD Eng

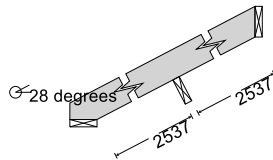
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## TIMBER RAFTER DESIGN (BS5268-2:2002)

TEDDS calculation version 1.0.03



### Rafter details

Breadth of timber sections;

$b = 47$  mm

Depth of timber sections;

$h = 175$  mm

Rafter spacing;

$s = 400$  mm

Rafter slope;

$\alpha = 27.5$  deg

Clear span of rafter on horizontal;

$L_{clh} = 2250$  mm

Clear span of rafter on slope;

$L_{cl} = L_{clh} / \cos(\alpha) = 2537$  mm

Rafter span;

**Continuous**

Timber strength class;

**C24**

### Section properties

Cross sectional area of rafter;

$A = b \times h = 8225$  mm<sup>2</sup>

Section modulus;

$Z = b \times h^2 / 6 = 239896$  mm<sup>3</sup>

Second moment of area;

$I = b \times h^3 / 12 = 20990885$  mm<sup>4</sup>

Radius of gyration;

$r = \sqrt{I / A} = 50.5$  mm

### Loading details

Rafter self weight;

$F_j = b \times h \times \rho_{char} \times g_{acc} = 0.03$  kN/m

Dead load on slope;

$F_d = 1.10$  kN/m<sup>2</sup>

Imposed load on plan;

$F_u = 0.75$  kN/m<sup>2</sup>

Imposed point load;

$F_p = 0.90$  kN

### Modification factors

Section depth factor;

$K_7 = (300 \text{ mm} / h)^{0.11} = 1.06$

Load sharing factor;

$K_8 = 1.10$

### Consider long term load condition

Load duration factor;

$K_3 = 1.00$

Total UDL perpendicular to rafter;

$F = F_d \times \cos(\alpha) \times s + F_j \times \cos(\alpha) = 0.415$  kN/m

Notional bearing length;

$L_b = F \times L_{cl} / [2 \times (b \times \sigma_{cp1} \times K_8 - F)] = 4$  mm

Effective span;

$L_{eff} = L_{cl} + L_b = 2541$  mm

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### Check bending stress at purlin

Bending stress parallel to grain;

$$\sigma_m = 7.500 \text{ N/mm}^2$$

Permissible bending stress;

$$\sigma_{m\_adm} = \sigma_m \times K_3 \times K_7 \times K_8 = 8.754 \text{ N/mm}^2$$

Applied bending stress;

$$\sigma_{m\_max} = F \times L_{eff}^2 / (8 \times Z) = 1.397 \text{ N/mm}^2$$

**PASS - Applied bending stress within permissible limits**

### Check compressive stress parallel to grain at purlin

Compression stress parallel to grain;

$$\sigma_c = 7.900 \text{ N/mm}^2$$

Minimum modulus of elasticity;

$$E_{min} = 7200 \text{ N/mm}^2$$

Compression member factor;

$$K_{12} = 0.73$$

Permissible compressive stress;

$$\sigma_{c\_adm} = \sigma_c \times K_3 \times K_8 \times K_{12} = 6.371 \text{ N/mm}^2$$

Applied compressive stress;

$$\sigma_{c\_max} = 3 \times F \times L_{eff} \times (\cot(\alpha) + 8 \times \tan(\alpha) / 3) / (8 \times A) = 0.159 \text{ N/mm}^2$$

**PASS - Applied compressive stress within permissible limits**

### Check combined bending and compressive stress parallel to grain at purlin

Euler stress;

$$\sigma_e = \pi^2 \times E_{min} / \lambda^2 = 28.091 \text{ N/mm}^2$$

Euler coefficient;

$$K_{eu} = 1 - (1.5 \times \sigma_{c\_max} \times K_{12} / \sigma_e) = 0.994$$

Combined axial compression and bending check;

$$\sigma_{m\_max} / (\sigma_{m\_adm} \times K_{eu}) + \sigma_{c\_max} / \sigma_{c\_adm} = 0.186; < 1$$

**PASS - Combined compressive and bending stresses are within permissible limits**

### Check bending stress in lower portion of rafter

Bending stress parallel to grain;

$$\sigma_m = 7.500 \text{ N/mm}^2$$

Permissible bending stress;

$$\sigma_{m\_adm} = \sigma_m \times K_3 \times K_7 \times K_8 = 8.754 \text{ N/mm}^2$$

Applied bending stress;

$$\sigma_{m\_max} = 9 \times F \times L_{eff}^2 / (128 \times Z) = 0.786 \text{ N/mm}^2$$

**PASS - Applied bending stress within permissible limits**

### Check compressive stress parallel to grain in lower portion of rafter

Compression stress parallel to grain;

$$\sigma_c = 7.900 \text{ N/mm}^2$$

Minimum modulus of elasticity;

$$E_{min} = 7200 \text{ N/mm}^2$$

Compression member factor;

$$K_{12} = 0.73$$

Permissible compressive stress;

$$\sigma_{c\_adm} = \sigma_c \times K_3 \times K_8 \times K_{12} = 6.371 \text{ N/mm}^2$$

Applied compressive stress;

$$\sigma_{c\_max} = 3 \times F \times L_{eff} \times (\cot(\alpha) + 13 \times \tan(\alpha) / 3) / (8 \times A) = 0.201 \text{ N/mm}^2$$

**PASS - Applied compressive stress within permissible limits**

### Check combined bending and compressive stress parallel to grain in lower portion of rafter

Euler stress;

$$\sigma_e = \pi^2 \times E_{min} / \lambda^2 = 28.091 \text{ N/mm}^2$$

Euler coefficient;

$$K_{eu} = 1 - (1.5 \times \sigma_{c\_max} \times K_{12} / \sigma_e) = 0.992$$

Combined axial compression and bending check;

$$\sigma_{m\_max} / (\sigma_{m\_adm} \times K_{eu}) + \sigma_{c\_max} / \sigma_{c\_adm} = 0.122; < 1$$

**PASS - Combined compressive and bending stresses are within permissible limits**

### Check shear stress

Shear stress parallel to grain;

$$\tau = 0.710 \text{ N/mm}^2$$

Permissible shear stress;

$$\tau_{adm} = \tau \times K_3 \times K_8 = 0.781 \text{ N/mm}^2$$

Applied shear stress;

$$\tau_{max} = 15 \times F \times L_{eff} / (16 \times A) = 0.120 \text{ N/mm}^2$$

**PASS - Applied shear stress within permissible limits**

### Check deflection

Permissible deflection;

$$\delta_{adm} = 0.003 \times L_{eff} = 7.623 \text{ mm}$$

Bending deflection;

$$\delta_b = F \times L_{eff}^4 / (185 \times E_{mean} \times I) = 0.413 \text{ mm}$$

Shear deflection;

$$\delta_s = 12 \times F \times L_{eff}^2 / (5 \times E_{mean} \times A) = 0.072 \text{ mm}$$

Total deflection;

$$\delta_{max} = \delta_b + \delta_s = 0.485 \text{ mm}$$

**PASS - Total deflection within permissible limits**



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### Consider medium term load condition

Load duration factor;

$$K_3 = 1.25$$

Total UDL perpendicular to rafter;

$$F = [F_u \times \cos(\alpha)^2 + F_d \times \cos(\alpha)] \times s + F_j \times \cos(\alpha) = 0.651 \text{ kN/m}$$

Notional bearing length;

$$L_b = F \times L_{cl} / [2 \times (b \times \sigma_{cp1} \times K_8 - F)] = 7 \text{ mm}$$

Effective span;

$$L_{eff} = L_{cl} + L_b = 2543 \text{ mm}$$

### Check bending stress at purlin

Bending stress parallel to grain;

$$\sigma_m = 7.500 \text{ N/mm}^2$$

Permissible bending stress;

$$\sigma_{m\_adm} = \sigma_m \times K_3 \times K_7 \times K_8 = 10.942 \text{ N/mm}^2$$

Applied bending stress;

$$\sigma_{m\_max} = F \times L_{eff}^2 / (8 \times Z) = 2.195 \text{ N/mm}^2$$

**PASS - Applied bending stress within permissible limits**

### Check compressive stress parallel to grain at purlin

Compression stress parallel to grain;

$$\sigma_c = 7.900 \text{ N/mm}^2$$

Minimum modulus of elasticity;

$$E_{min} = 7200 \text{ N/mm}^2$$

Compression member factor;

$$K_{12} = 0.71$$

Permissible compressive stress;

$$\sigma_{c\_adm} = \sigma_c \times K_3 \times K_8 \times K_{12} = 7.739 \text{ N/mm}^2$$

Applied compressive stress;

$$\sigma_{c\_max} = 3 \times F \times L_{eff} \times (\cot(\alpha) + 8 \times \tan(\alpha) / 3) / (8 \times A) = 0.250 \text{ N/mm}^2$$

**PASS - Applied compressive stress within permissible limits**

### Check combined bending and compressive stress parallel to grain at purlin

Euler stress;

$$\sigma_e = \pi^2 \times E_{min} / \lambda^2 = 28.037 \text{ N/mm}^2$$

Euler coefficient;

$$K_{eu} = 1 - (1.5 \times \sigma_{c\_max} \times K_{12} / \sigma_e) = 0.990$$

Combined axial compression and bending check;

$$\sigma_{m\_max} / (\sigma_{m\_adm} \times K_{eu}) + \sigma_{c\_max} / \sigma_{c\_adm} = 0.235; < 1$$

**PASS - Combined compressive and bending stresses are within permissible limits**

### Check bending stress in lower portion of rafter

Bending stress parallel to grain;

$$\sigma_m = 7.500 \text{ N/mm}^2$$

Permissible bending stress;

$$\sigma_{m\_adm} = \sigma_m \times K_3 \times K_7 \times K_8 = 10.942 \text{ N/mm}^2$$

Applied bending stress;

$$\sigma_{m\_max} = 9 \times F \times L_{eff}^2 / (128 \times Z) = 1.235 \text{ N/mm}^2$$

**PASS - Applied bending stress within permissible limits**

### Check compressive stress parallel to grain in lower portion of rafter

Compression stress parallel to grain;

$$\sigma_c = 7.900 \text{ N/mm}^2$$

Minimum modulus of elasticity;

$$E_{min} = 7200 \text{ N/mm}^2$$

Compression member factor;

$$K_{12} = 0.71$$

Permissible compressive stress;

$$\sigma_{c\_adm} = \sigma_c \times K_3 \times K_8 \times K_{12} = 7.739 \text{ N/mm}^2$$

Applied compressive stress;

$$\sigma_{c\_max} = 3 \times F \times L_{eff} \times (\cot(\alpha) + 13 \times \tan(\alpha) / 3) / (8 \times A) = 0.315 \text{ N/mm}^2$$

**PASS - Applied compressive stress within permissible limits**

### Check combined bending and compressive stress parallel to grain in lower portion of rafter

Euler stress;

$$\sigma_e = \pi^2 \times E_{min} / \lambda^2 = 28.037 \text{ N/mm}^2$$

Euler coefficient;

$$K_{eu} = 1 - (1.5 \times \sigma_{c\_max} \times K_{12} / \sigma_e) = 0.988$$

Combined axial compression and bending check;

$$\sigma_{m\_max} / (\sigma_{m\_adm} \times K_{eu}) + \sigma_{c\_max} / \sigma_{c\_adm} = 0.155; < 1$$

**PASS - Combined compressive and bending stresses are within permissible limits**

### Check shear stress

Shear stress parallel to grain;

$$\tau = 0.710 \text{ N/mm}^2$$

Permissible shear stress;

$$\tau_{adm} = \tau \times K_3 \times K_8 = 0.976 \text{ N/mm}^2$$

Applied shear stress;

$$\tau_{max} = 15 \times F \times L_{eff} / (16 \times A) = 0.189 \text{ N/mm}^2$$

**PASS - Applied shear stress within permissible limits**

### Check deflection

Permissible deflection;

$$\delta_{adm} = 0.003 \times L_{eff} = 7.630 \text{ mm}$$

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Bending deflection;

$$\delta_b = F \times L_{eff}^4 / (185 \times E_{mean} \times I) = \mathbf{0.650 \text{ mm}}$$

Shear deflection;

$$\delta_s = 12 \times F \times L_{eff}^2 / (5 \times E_{mean} \times A) = \mathbf{0.114 \text{ mm}}$$

Total deflection;

$$\delta_{max} = \delta_b + \delta_s = \mathbf{0.764 \text{ mm}}$$

**PASS - Total deflection within permissible limits**

### Consider short term load condition

Load duration factor;

$$K_3 = \mathbf{1.50}$$

Total UDL perpendicular to rafter;

$$F = F_d \times \cos(\alpha) \times s + F_j \times \cos(\alpha) = \mathbf{0.415 \text{ kN/m}}$$

Notional bearing length;

$$L_b = [F \times L_{cl} + F_p \times \cos(\alpha)] / [2 \times (b \times \sigma_{cp1} \times K_8 - F)] = \mathbf{7 \text{ mm}}$$

Effective span;

$$L_{eff} = L_{cl} + L_b = \mathbf{2544 \text{ mm}}$$

### Check bending stress at purlin

Bending stress parallel to grain;

$$\sigma_m = \mathbf{7.500 \text{ N/mm}^2}$$

Permissible bending stress;

$$\sigma_{m\_adm} = \sigma_m \times K_3 \times K_7 \times K_8 = \mathbf{13.131 \text{ N/mm}^2}$$

Applied bending stress;

$$\sigma_{m\_max} = F \times L_{eff}^2 / (8 \times Z) + 3 \times F_p \times \cos(\alpha) \times L_{eff} / (32 \times Z) = \mathbf{2.194 \text{ N/mm}^2}$$

**PASS - Applied bending stress within permissible limits**

### Check compressive stress parallel to grain at purlin

Compression stress parallel to grain;

$$\sigma_c = \mathbf{7.900 \text{ N/mm}^2}$$

Minimum modulus of elasticity;

$$E_{min} = \mathbf{7200 \text{ N/mm}^2}$$

Compression member factor;

$$K_{12} = \mathbf{0.69}$$

Permissible compressive stress;

$$\sigma_{c\_adm} = \sigma_c \times K_3 \times K_8 \times K_{12} = \mathbf{9.001 \text{ N/mm}^2}$$

Applied compressive stress;

$$\sigma_{c\_max} = 3 \times F \times L_{eff} \times (\cot(\alpha) + 8 \times \tan(\alpha) / 3) / (8 \times A) + F_p \times \sin(\alpha) / A = \mathbf{0.210 \text{ N/mm}^2}$$

**PASS - Applied compressive stress within permissible limits**

### Check combined bending and compressive stress parallel to grain at purlin

Euler stress;

$$\sigma_e = \pi^2 \times E_{min} / \lambda^2 = \mathbf{28.019 \text{ N/mm}^2}$$

Euler coefficient;

$$K_{eu} = 1 - (1.5 \times \sigma_{c\_max} \times K_{12} / \sigma_e) = \mathbf{0.992}$$

Combined axial compression and bending check;

$$\sigma_{m\_max} / (\sigma_{m\_adm} \times K_{eu}) + \sigma_{c\_max} / \sigma_{c\_adm} = \mathbf{0.192; < 1}$$

**PASS - Combined compressive and bending stresses are within permissible limits**

### Check bending stress in lower portion of rafter

Bending stress parallel to grain;

$$\sigma_m = \mathbf{7.500 \text{ N/mm}^2}$$

Permissible bending stress;

$$\sigma_{m\_adm} = \sigma_m \times K_3 \times K_7 \times K_8 = \mathbf{13.131 \text{ N/mm}^2}$$

Applied bending stress;

$$\sigma_{m\_max} = F \times L_{eff}^2 / (16 \times Z) + 13 \times F_p \times \cos(\alpha) \times L_{eff} / (64 \times Z) = \mathbf{2.420 \text{ N/mm}^2}$$

**PASS - Applied bending stress within permissible limits**

### Check compressive stress parallel to grain in lower portion of rafter

Compression stress parallel to grain;

$$\sigma_c = \mathbf{7.900 \text{ N/mm}^2}$$

Minimum modulus of elasticity;

$$E_{min} = \mathbf{7200 \text{ N/mm}^2}$$

Compression member factor;

$$K_{12} = \mathbf{0.69}$$

Permissible compressive stress;

$$\sigma_{c\_adm} = \sigma_c \times K_3 \times K_8 \times K_{12} = \mathbf{9.001 \text{ N/mm}^2}$$

Applied compressive stress;

$$\sigma_{c\_max} = 3 \times F \times L_{eff} \times (\cot(\alpha) + 4 \times \tan(\alpha)) / (8 \times A) + F_p \times \sin(\alpha) / A = \mathbf{0.243 \text{ N/mm}^2}$$

**PASS - Applied compressive stress within permissible limits**

### Check combined bending and compressive stress parallel to grain in lower portion of rafter

Euler stress;

$$\sigma_e = \pi^2 \times E_{min} / \lambda^2 = \mathbf{28.019 \text{ N/mm}^2}$$

Euler coefficient;

$$K_{eu} = 1 - (1.5 \times \sigma_{c\_max} \times K_{12} / \sigma_e) = \mathbf{0.991}$$

Combined axial compression and bending check;

$$\sigma_{m\_max} / (\sigma_{m\_adm} \times K_{eu}) + \sigma_{c\_max} / \sigma_{c\_adm} = \mathbf{0.213; < 1}$$

**PASS - Combined compressive and bending stresses are within permissible limits**

### Check shear stress

Shear stress parallel to grain;

$$\tau = \mathbf{0.710 \text{ N/mm}^2}$$

Permissible shear stress;

$$\tau_{adm} = \tau \times K_3 \times K_8 = \mathbf{1.172 \text{ N/mm}^2}$$

Applied shear stress;

$$\tau_{max} = 15 \times F \times L_{eff} / (16 \times A) + 3 \times F_p \times \cos(\alpha) / (2 \times A) = \mathbf{0.266 \text{ N/mm}^2}$$

# WDcEng

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**PASS - Applied shear stress within permissible limits**

**Check deflection**

Permissible deflection;

$$\delta_{adm} = 0.003 \times L_{eff} = \mathbf{7.632 \text{ mm}}$$

Bending deflection;

$$\delta_b = L_{eff}^3 \times (F \times L_{eff} / 185 + 0.015 \times F_p \times \cos(\alpha)) / (E_{mean} \times I) = \mathbf{1.285 \text{ mm}}$$

Shear deflection;

$$\delta_s = 12 \times L_{eff} \times (F \times L_{eff} + 2 \times F_p \times \cos(\alpha)) / (5 \times E_{mean} \times A) = \mathbf{0.182 \text{ mm}}$$

Total deflection;

$$\delta_{max} = \delta_b + \delta_s = \mathbf{1.467 \text{ mm}}$$

**PASS - Total deflection within permissible limits**

;