

SM Design & Consulting Ltd

Consulting Structural and Design Engineers

28/11/22

Your Ref:

Our Ref: 22-251

Contact: Simon Maddox

Email: simon@smdesignconsult.co.uk

CALCULATIONS FOR: LITTLE PAXTON VILLAGE HALL

PROPOSAL: These calculations have been prepared for new office building.

CODES USED:

- BS 648, 1964: Weights of Building Materials
- BS 6399 Part 1, 1996: Loads for Buildings; Dead & Imposed Loads
- BS 6399 Part 2, 1997: Loads for Buildings; Wind Loads
- BS 5950 Part 1, 2000: Structural Use of Steelwork in Building
- BS 8110 Part 1, 1997: Structural Use of Concrete
- BS 5268 Part 2, 2002: Structural Use of Timber
- BS 5628 Part 1, 2005: Structural Use of Masonry

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Loads for Roofs

kg/m² Dead

Live

Tiled Roof –

Tiles (standard clay)
Felt and battens
Rafters

75
6
6

**Plan Load Total
Pitch 45**

87

1.23

0.60

Tiled Roof (with lining) –

Tiles (standard clay)
Felt and battens
Rafters
Battens & insulation
Plasterboard & skim

75
6
6
4
15

**Plan Load Total
Pitch 45**

106

1.65

0.60

Built up felt roof (flat roof) -

Felt & chippings
Board & insulation
Joists & firings
Plasterboard & skim

40
15
10
15

Total

80

0.80

0.75

(with access)

1.50

Ceilings –

Joists
Insulation
Plasterboard & skim

8
2
15

Total

25

0.25

0.25

Timber Floors –

Boarding
Joists
Insulation
Plasterboard & skim

20
8
2
15

Total

45

0.45

1.50

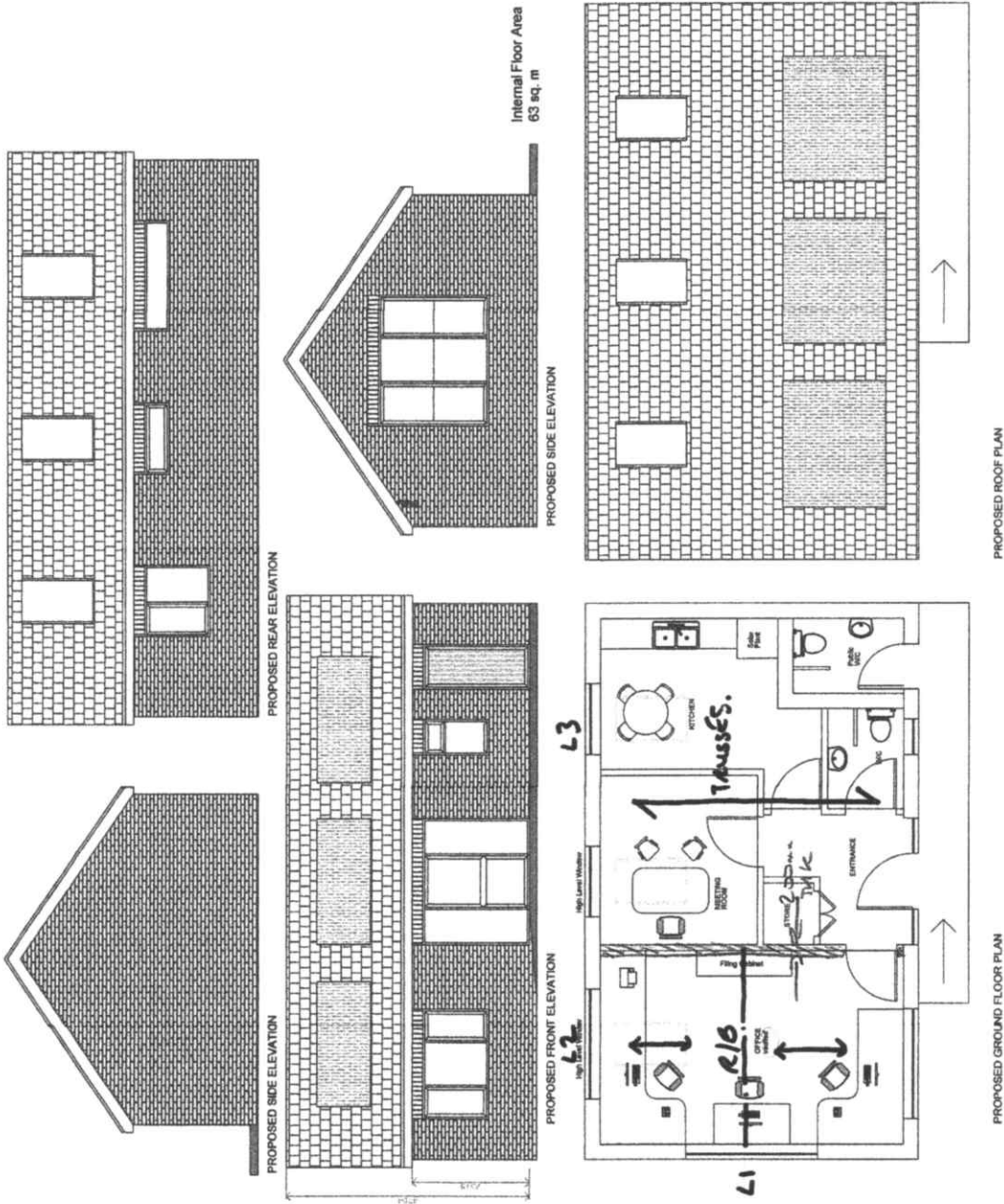
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Loads for Walls

	kg/m ² Dead	Live
New cavity walls -		
102 brick	210	
100 block	80	
12mm plaster	24	
Total	314 3.14	-
New party walls -		
100 block	160	
100 block	160	
2 x 12mm plaster	48	
Total	368 3.68	-
Internal block walls -		
100 block	160	
2 x 12mm plaster	48	
Total	208 2.08	-
Stud Partition walls –		
2 x 9.5mm Plasterboard	20	
2 x skim coat plaster	10	
Studs 75 x 50 @ 400c/c	10	
Total	40 0.40	-

NOTES - Drainage subject to a visit by the builder and assessment of existing drains. Party wall act may be required and is the responsibility of the homeowner, we can advise if required. Please review our Terms and Conditions on our website www.binneyandsonsdesign.co.uk Site plans and Location plans purchased from streetwise.net and are subject to their terms and conditions. Drawings are for planning purposes only. Prior to commencement of works the contractor is responsible for checking the plans to the site conditions, if any anomalies are found they are reported for rectification. Failure to do so at this stage will result in the contractor being liable for resulting costs incurred. Drawings are subject to structural engineering and building control. Copyright— © 2022		Client:	Little Paxton Parish Council
		Site Address:	Village Hall Car Park Little Paxton St Neots PE19
		Scale:	1/100
		Drawn By:	PS
		Date:	9th November 2022
		Drawing No:	730/3 PRO
		Z:\Support Files\B&S Logo.gif	



PROJECT Village Hall Car Park, Little Paxton, St Neots

STRUCTURAL DESIGNLINTERSii) L1 span = 2.5m

$$\begin{array}{lcl} \text{Roof} & 2 \times 6/2 \times 4/2 & = 4.0 \text{ kN/m} \\ \text{wall} & & = 4.0 \text{ kN/m} \end{array}$$

$$\underline{8.0 \text{ kN/m}}$$

$$8 \times 2.5 = \underline{20 \text{ kN}}$$

$$\underline{16 \text{ L1/40}} \quad (35)$$

(ii) L2 span = 2.3m

$$\begin{array}{lcl} \text{Roof} & 2 \times 3/2 & 3.00 \\ \text{wall} & & 1.00 \\ \hline & & 4.00 \end{array}$$

$$4 \times 2.3 = 9.20$$

$$\underline{16 \text{ L2/5}} \quad (22)$$

(iii) L3

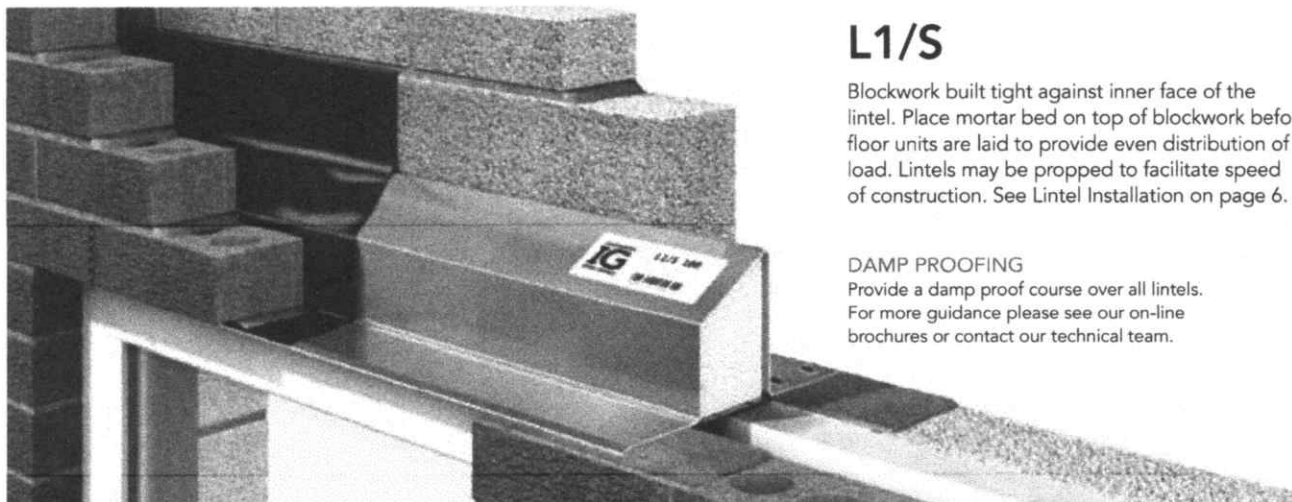
$$\begin{array}{lcl} \text{Roof} & 2 \times 6/2 & 6.0 \\ \text{wall} & & 1.0 \\ \hline & & 7.0 \end{array}$$

$$7.0 \times 2.5 = 17.5 \text{ kN}$$

$$\underline{16 \text{ L3/5}} \quad (22)$$

Cavity Wall

Available for cavity widths from 50mm to 165mm



OUTER LEAF

102mm

INNER LEAF

100mm

L1/S

Blockwork built tight against inner face of the lintel. Place mortar bed on top of blockwork before floor units are laid to provide even distribution of load. Lintels may be propped to facilitate speed of construction. See Lintel Installation on page 6.

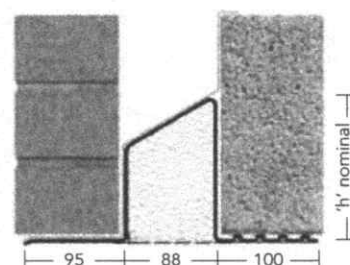
DAMP PROOFING

Provide a damp proof course over all lintels. For more guidance please see our on-line brochures or contact our technical team.

Standard Load

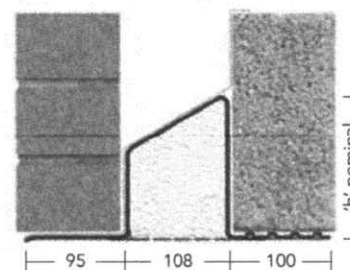
L1/S 100 For cavity widths 90-105mm										
Manufactured length 150mm increments	600- 1200	1350- 1500	1650- 1800	1950- 2100	2250- 2400	2550- 2700	2850- 3000	3150- 3600	3750- 4050	4200- 4800
Height 'h'	88	88	107	125	150	162	171	200	200	200
Thickness	1.6	2.0	2.0	2.0	2.0	2.6	2.6	3.2	3.2	3.4
Total UDL kN 3:1	12	16	19	21	23	27	27	27	26	27
Total UDL kN 19:1	10	13	16	17	18	22	20	20	19	22

90-105mm cavity



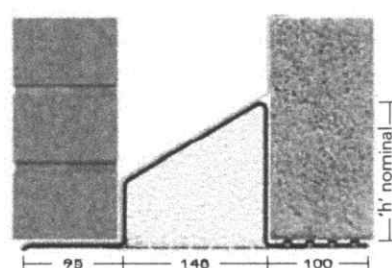
L1/S 110 For cavity widths 110-125mm						
Manufactured length 150mm increments	600- 1500	1650- 1800	1950- 2100	2250- 3000	3150- 4050	4200- 4800
Height 'h'	95	121	145	195	195	195
Thickness	2.0	2.0	2.6	2.9	3.2	3.4
Total UDL kN 3:1	16	22	24	27	26	25
Total UDL kN 19:1	13	18	18	22	19	20

110-125mm cavity



L1/S 150 For cavity widths 150-165mm						
Manufactured length 150mm increments	600- 1500	1650- 1800	1950- 2100	2250- 3000	3150- 4050	4200- 4800
Height 'h'	100	125	180	180	180	180
Thickness	2.0	2.0	2.6	2.9	3.2	3.4
Total UDL kN 3:1	16	22	24	27	26	25
Total UDL kN 19:1	13	18	18	22	19	20

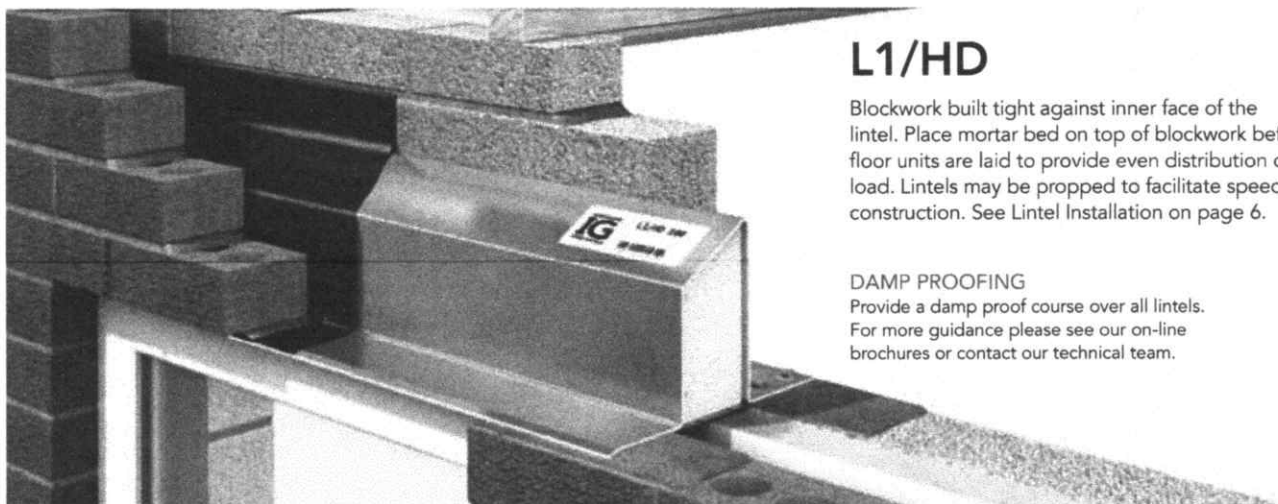
150-165mm cavity



Please note other cavity widths and loading conditions are available.

Cavity Wall

Available for cavity widths from 50mm to 165mm



OUTER LEAF

102mm

INNER LEAF

100mm

L1/HD

Blockwork built tight against inner face of the lintel. Place mortar bed on top of blockwork before floor units are laid to provide even distribution of load. Lintels may be propped to facilitate speed of construction. See Lintel Installation on page 6.

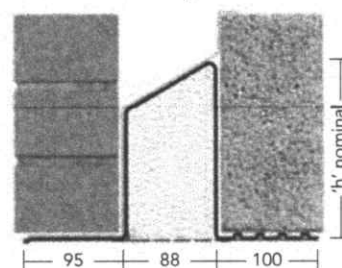
DAMP PROOFING

Provide a damp proof course over all lintels. For more guidance please see our on-line brochures or contact our technical team.

Heavy Duty Load

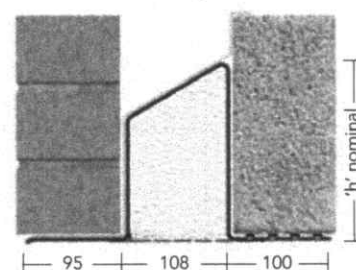
L1/HD 100 For cavity widths 90-105mm							
Manufactured length 150mm increments	600- 1200	1350- 1500	1650- 2100	2250- 2550	2700- 3000	3150- 3600	3750- 4200
Height 'h'	110	135	163	203	203	203	203
Thickness	2.9	2.9	2.9	2.9	3.2	3.2	3.2
Total UDL kN 3:1	30	30	40	40	40	35	33
Total UDL kN 19:1	22	22	35	35	35	32	28

90-105mm cavity



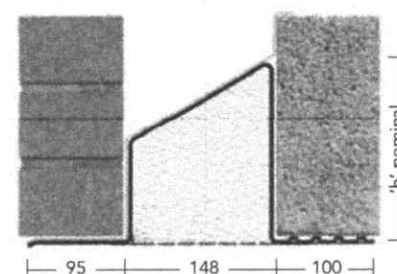
L1/HD 110 For cavity widths 110-125mm					
Manufactured length 150mm increments	600- 1500	1650- 2100	2250- 3000	3150- 3600	3750- 4050
Height 'h'	125	145	195	195	195
Thickness	2.9	2.9	2.9	3.2	3.2
Total UDL kN 3:1	30	30	35	32	30
Total UDL kN 19:1	20	22	30	28	26

110-125mm cavity



L1/HD 150 For cavity widths 150-165mm					
Manufactured length 150mm increments	600- 1500	1650- 2100	2250- 3000	3150- 3600	3750- 4050
Height 'h'	125	160	180	180	200
Thickness	2.9	2.9	3.2	3.2	3.2
Total UDL kN 3:1	30	30	35	30	30
Total UDL kN 19:1	20	22	30	25	26

150-165mm cavity



Please note other cavity widths and loading conditions are available.

PROJECT Village Hall Car Park, Little Paxton, St Neots

(iv) RAFTERS

SPAN = 3.5m

TRUSS 6-18

$$\frac{50 \times 175 \text{ C24}}{0.4000 \text{ C/S}}$$

(8.2m)

(v) RIDGE BEAM

SPAN = 4.0m

(Kiln)

OW

0.30

ROOF 1.2 x 6/2
0.75 x 6/2

3.60

2.25

3.90

2.25

FOUNDATIONS

BGS MAP INDICATES RIVER TERRACE
DEPOSITS OVER OXFORD CLAY. FOOTINGS
600mm WIDE & MIN 1000mm DD SUBJECT
TO LA INSPECTION & APPROVAL ON SITE.

Table 6.17 Permissible clear spans for common or jack raftersSlope of roof 30.0° or more but less than 45.0° Imposed load $F_i = 0.75 \text{ kN/m}^2$

Single span

Strength Class C16

Service Class 1 or 2

		Dead loads F_d (kN/m ²)								
		F_d not more than 0.5			F_d more than 0.5 but not more than 0.75			F_d more than 0.75 but not more than 1.00		
Size of rafter		Spacing of rafters (mm)								
Breadth (mm)	Depth (mm)	400	450	600	400	450	600	400	450	600
		Maximum clear span (m)								
38	100	2.30	2.24	2.11	2.11	2.06	1.91	1.97	1.91	1.77
38	125	3.09	2.97	2.70	2.89	2.78	2.52	2.67	2.58	2.36
38	150	3.70	3.56	3.23	3.46	3.33	3.03	3.28	3.15	2.86
38	195	4.78	4.60	4.19	4.49	4.32	3.92	4.25	4.09	3.68
44	100	2.57	2.50	2.27	2.35	2.29	2.12	2.19	2.12	1.95
44	125	3.24	3.12	2.83	3.04	2.92	2.65	2.88	2.76	2.51
44	150	3.88	3.73	3.39	3.64	3.50	3.18	3.44	3.31	3.01
44	195	5.01	4.83	4.40	4.71	4.53	4.12	4.46	4.29	3.90
47	100	2.66	2.55	2.32	2.47	2.39	2.17	2.29	2.22	2.04
47	125	3.31	3.18	2.90	3.10	2.98	2.71	2.94	2.83	2.57
47	150	3.96	3.81	3.47	3.71	3.57	3.25	3.52	3.39	3.08
47	195	5.12	4.93	4.49	4.81	4.63	4.21	4.56	4.39	3.99
ALS/CLS										
38	89	1.92	1.88	1.78	1.78	1.74	1.63	1.67	1.63	1.51
38	140	3.45	3.32	3.02	3.24	3.11	2.83	3.06	2.95	2.67
38	184	4.52	4.35	3.96	4.24	4.08	3.70	4.01	3.86	3.48

Table 6.18 Permissible clear spans for common or jack raftersSlope of roof 30.0° or more but less than 45.0° Imposed load $F_i = 0.75 \text{ kN/m}^2$

Single span

Strength Class C24

Service Class 1 or 2

Size of rafter		Dead loads F_d (kN/m ²)									
		F_d not more than 0.5			F_d more than 0.5 but not more than 0.75			F_d more than 0.75 but not more than 1.00			
Spacing of rafters (mm)		Maximum clear span (m)									
Breadth (mm)	Depth (mm)	400	450	600	400	450	600	400	450	600	
ALS/CLS	38	100	2.65	2.55	2.32	2.48	2.39	2.17	2.35	2.26	2.05
	38	125	3.30	3.18	2.89	3.10	2.98	2.71	2.93	2.82	2.56
	38	150	3.95	3.81	3.46	3.71	3.57	3.24	3.51	3.38	3.07
	38	195	5.11	4.92	4.49	4.80	4.62	4.20	4.55	4.38	3.98
	44	100	2.78	2.68	2.43	2.61	2.51	2.28	2.47	2.37	2.16
	44	125	3.47	3.34	3.03	3.25	3.13	2.84	3.08	2.96	2.69
	44	150	4.14	3.99	3.63	3.89	3.74	3.40	3.69	3.55	3.22
	44	195	5.36	5.16	4.71	5.03	4.85	4.41	4.77	4.59	4.18
	47	100	2.84	2.73	2.49	2.66	2.56	2.33	2.52	2.43	2.20
	47	125	3.54	3.41	3.10	3.32	3.20	2.91	3.15	3.03	2.75
	47	150	4.23	4.08	3.71	3.97	3.82	3.48	3.77	3.62	3.29
	47	195	5.47	5.27	4.81	5.14	4.95	4.51	4.88	4.69	4.27
	38	89	2.36	2.27	2.06	2.21	2.13	1.93	2.09	2.01	1.83
	38	140	3.69	3.56	3.23	3.46	3.33	3.03	3.28	3.16	2.86
	38	184	4.83	4.65	4.24	4.53	4.36	3.97	4.30	4.13	3.76

SM Design & Consulting Ltd
07939 595055

Site: Little Paxton Village Hall

Job: Calcs

Job number: 22-251

ProSteel 7.05b 532145

Made by SAM

Page 09

File copy

Printed 28 Nov 2022 14:58

Beam: Ridge Beam

Span: 4.0 m.

Load name	Loading w1	Start x1	Loading w2	End x2	R1comp	R2comp
U D dl	4	0		L	8.00	8.00
U L ll	2.25	0		L	4.50	4.50
Unfactored reactions (kN) Total:					12.50	12.50
Dead:					8.00	8.00
Live:					4.50	4.50
Factored reactions:					18.40	18.40

Total load: 25.00/36.80 kN Unfactored/Factored

Factored reactions:

Load types: U: UDL D: Dead; L: Live (positions in m. from R1)

Maximum B.M. (factored) = 18.40 kNm at 2.00 m. from R1

Maximum S.F. (factored) = 18.40 kN at 0.00 m. from R1

Live load deflection = $7.50 \times 10^8 / EI$ at 2.00 m. from R1 (E in N/mm^2 , I in cm^4)

Total deflection = $20.8 \times 10^8 / EI$ at 2.00 m. from R1

Beam calculation to BS5950-1:2000 using S275 steel

SECTION SIZE : 203 x 133 x 30 UB S275 (compact)

D=206.8 mm B=133.9 mm t=6.4 mm T=9.6 mm $I_x=2,900 \text{ cm}^4$ $r_y=3.17 \text{ cm}$ $S_x=314 \text{ cm}^3$ $x=21.5$

Shear

Shear capacity = $0.6 p_y t D = 0.6 \times 275 \times 6.4 \times 206.8 / 1000 = 218 \text{ kN}$ (≥ 18.4) OK

Bending

Maximum moment = 18.40 kNm at 2.00 m. from R1

Moment capacity, $M_c = p_y S_x = 275 \times 314 / 1000 = 86.35 \text{ kNm}$ OK

Lateral-torsional buckling

Beam is laterally restrained at supports only

Restraint condition at R1 and R2: Compression flange laterally unrestrained; both flanges free to rotate on plan.

Partial torsional restraint by dead bearing of bottom flange to support (1.2L+2D) [BS5950 Table 13]

Effective length = 1.2L+2D

Bending strength, $p_b = 120.0 \text{ N/mm}^2$

Maximum moment within segment, $M_x = 18.40 \text{ kNm}$

Equivalent uniform moment factor, $m_{LT} = 0.925$ ($M_2=13.8$, $M_3=18.4$, $M_4=13.8$)

Equivalent uniform moment = $0.925 \times 18.40 = 17.02 \text{ kNm}$

Buckling resistance moment, $M_b = p_b S_x = 120.0 \times 314 / 1000 = 37.67 \text{ kNm}$ OK

Web capacity

Check unstiffened web capacity with load of 18.40 kN

$C1 = 60.5 \text{ kN}$; $C2 = 1.76 \text{ kN/mm}$; $C4 = 261$; $K = \min\{0.5 + (a_e / 1.4d), 1.0\}$; $p_{vw} = 275 \text{ N/mm}^2$
(for derivation of C factors see Steelwork Design Guide to BS5950-1:2000 6th ed.)

Minimum required stiff bearing length, $b_1 = 0 \text{ mm}$; $a_e = 0 \text{ mm}$; $K = 0.500$

Bearing capacity, $P_w = C1 + b_1 C2 = 60.5 \text{ kN} \lll$

Buckling capacity, $P_x = K / (C4 P_w) = 0.500 / (261 \times 60.5) = 62.9 \text{ kN}$

Deflection

LL deflection = $7.50 \times 1e8 / 205,000 \times 2,900 = 1.3 \text{ mm}$ (L/3171) OK

TL deflection = $20.8 \times 1e8 / 205,000 \times 2,900 = 3.5 \text{ mm}$ (L/1142)