

Your name goes here

Your address goes here

Site: Land Adjacent to Park House, Glenfield

Job: New Maintenance Building

Job number: 7406

SuperBeam 7.03a 440365

Made by SG

Page 5

File copy

Noname.SBW

Printed 21 Mar 2018 14:26

Beam: Beam 1

Span: 9.1 m.

	Load name	Loading w1	Start x1	Loading w2	End x2	R1comp	R2comp
U D	o.w.	2.4	0		L	10.92	10.92
U D	Roof	8.52	0		L	38.77	38.77
				Total load: 99.37 kN		49.69	49.69
				Dead:		49.69	49.69
				Live:		0.00	0.00

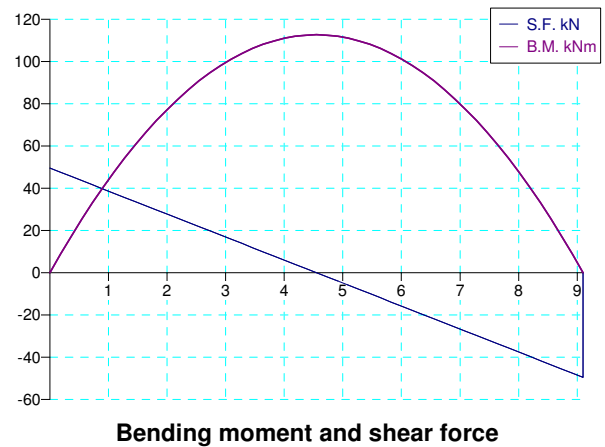
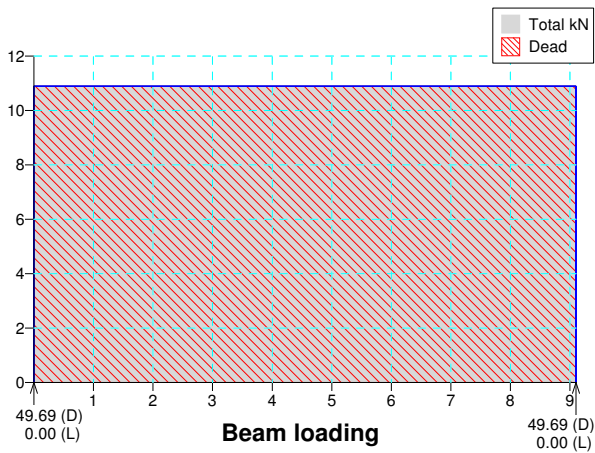
Load types: U: UDL D: Dead; L: Live (positions in m. from R1)

Maximum B.M. = 113 kNm at 4.55 m. from R1

Maximum S.F. = -49.7 kN at R2

Live load deflection = $0.00 \times 10^8 / EI$ at R2 (E in N/mm^2 , I in cm^4)

Total deflection = $975 \times 10^8 / EI$ at 4.55 m. from R1



Your name goes here

Your address goes here

Site: Land Adjacent to Park House, Glenfield

Job: New Maintenance Building

Job number: 7406

SuperBeam 7.03a 440365

Made by SG

Page 6

File copy

Noname.SBW Printed 21 Mar 2018 14:26

Beam: Beam 1

Span: 9.1 m.

	Load name	Loading w1	Start x1	Loading w2	End x2	R1comp	R2comp
U D	o.w.	2.4	0		L	10.92	10.92
U D	Roof	8.52	0		L	38.77	38.77
Total load: 99.37 kN						49.69	49.69
Dead:						49.69	49.69
Live:						0.00	0.00

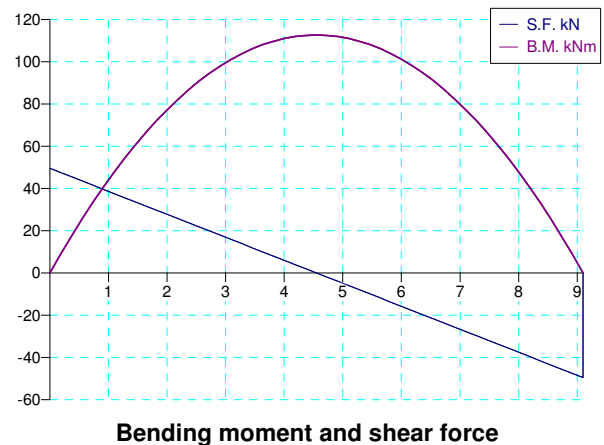
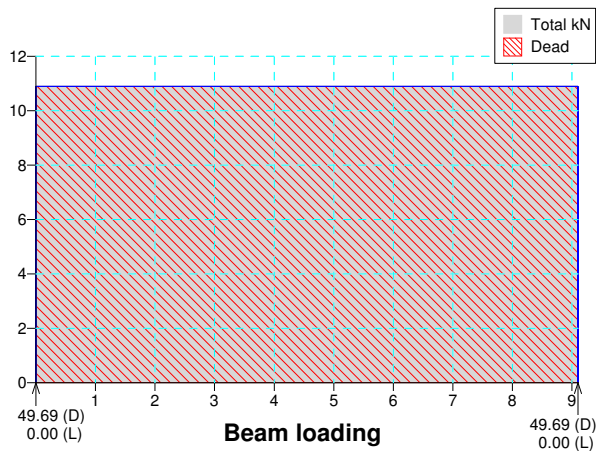
Load types: U: UDL D: Dead; L: Live (positions in m. from R1)

Maximum B.M. = 113 kNm at 4.55 m. from R1

Maximum S.F. = -49.7 kN at R2

Live load deflection = $0.00 \times 10^8 / EI$ at R2 (E in N/mm^2 , I in cm^4)

Total deflection = $975 \times 10^8 / EI$ at 4.55 m. from R1



Steel beam calculation to BS449 Part 2 using S355 steel

SECTION SIZE : 305 x 305 x 198 UC S355

D=339.9 mm B=314.5 mm t=19.1 mm T=31.4 mm $I_x=50,900 \text{ cm}^4$ $r_y=8.04 \text{ cm}$ $Z_x=3,000 \text{ cm}^3$

Bending: $L_E/r_y = 9.10 \times 100/8.04 = 113$ D/T = 10.8

Permissible bending stress, $p_{bc} = 187.3 \text{ N/mm}^2$ (Table 3b)

Actual bending stress, $f_{bc} = 113.0 \times 1000/3000.0 = 37.7 \text{ N/mm}^2$ OK

Shear: Maximum shear in web, $f_s = 49.7 \times 1000/(19.1 \times 339.9) = 7.7 \text{ N/mm}^2$ OK

Beam web: Check unstiffened web capacity with load of 49.69 kN

Bearing: $p_b = 260 \text{ N/mm}^2$ (Table 9); C1 = 401 kN; C2 = 4.97 kN/mm

Buckling: $p_c = 204 \text{ N/mm}^2$ (Table 17b); C1 = 661 kN; C2 = 3.89 kN/mm

Minimum required stiff bearing length, $L_b = 0 \text{ mm}$

Bearing capacity, $P_w = C1 + L_b \cdot C2 = 401 \text{ kN} \ll$

Buckling capacity, $P_x = C1 + L_b \cdot C2 = 661 \text{ kN}$

Deflection: Live load deflection = $0.00 \times 1e8/(205,000 \times 50,900) = 0.0 \text{ mm}$ OK

Total deflection = $975 \times 1e8/(205,000 \times 50,900) = 9.3 \text{ mm}$ (L/974)

Combined bending and shear check (14.c): $(f_{bc}/p_{bc})^2 + (f_s/p_s)^2 = 0.040$ at 4.55 m. (≤ 1.25 OK)

Your name goes here

Your address goes here

Site: Land Adjacent to Park House, Glenfield

Job: New Maintenance Building

Job number: 7406

Made by SG

Page 7

File copy

SuperBeam 7.03a 440365

Noname.SBW Printed 21 Mar 2018 14:26

Bearings

305 x 305 x 198 UC stiff bearing length, $b_1 = t + 1.6r + 2T = 106.2$ mm

Masonry: 100mm 3.6N/mm² solid block (SF>2.0), class (iii) mortar, normal const/normal mfr

Local design strength (factored) = $3.5/3.5 = 1.00$ N/mm² (BS5628-1:2005 Table 2d/2e)

R1: 700 x 100 mm padstone

Factored reaction = $49.69 \times 1.4 + 0.00 \times 1.6 = 69.56$ kN

Factored stress under padstone = $69.56 \times 1000/700 \times 100 = 0.99$ N/mm²

R2 as R1

Your name goes here

Your address goes here

Site: Land Adjacent to Park House, Glenfield

Job: New Maintenance Building

Job number: 7406

SuperBeam 7.03a 440365

Made by SG

Page 8

File copy

Noname.SBW Printed 21 Mar 2018 14:26

Beam: Beam 1

9.1 m. span

Section : 305 x 305 x 198 UC S355

Zxx = 3,000 cm³ Shear area = 6,492 mm²

Analysis (all loads applied)

<i>From</i>	<i>B.M.</i>	<i>f_{bc}</i>	<i>S.F.</i>	<i>f_s</i>	<i>Deflection mm.</i>		
<i>R1 m.</i>	<i>kNm</i>	<i>N/mm²</i>	<i>kN</i>	<i>N/mm²</i>	<i>Dead</i>	<i>Live</i>	<i>Total</i>
0.000	0.0	0.00	49.69	7.653	0.00	0.00	0.00
0.455	21.5	7.16	44.72	6.888	1.49	0.00	1.49
0.910	40.7	13.56	39.75	6.123	2.93	0.00	2.93
1.365	57.6	19.22	34.78	5.357	4.30	0.00	4.30
1.820	72.3	24.11	29.81	4.592	5.55	0.00	5.55
2.275	84.8	28.26	24.84	3.827	6.66	0.00	6.66
2.730	94.9	31.65	19.87	3.061	7.60	0.00	7.60
3.185	102.9	34.29	14.91	2.296	8.35	0.00	8.35
3.640	108.5	36.17	9.94	1.531	8.90	0.00	8.90
4.095	111.9	37.30	4.97	0.765	9.23	0.00	9.23
4.550	113.0	37.68	0.00	0.000	9.34	0.00	9.34
5.005	111.9	37.30	-4.97	-0.765	9.23	0.00	9.23
5.460	108.5	36.17	-9.94	-1.531	8.90	0.00	8.90
5.915	102.9	34.29	-14.91	-2.296	8.35	0.00	8.35
6.370	94.9	31.65	-19.87	-3.061	7.60	0.00	7.60
6.825	84.8	28.26	-24.84	-3.827	6.66	0.00	6.66
7.280	72.3	24.11	-29.81	-4.592	5.55	0.00	5.55
7.735	57.6	19.22	-34.78	-5.357	4.30	0.00	4.30
8.190	40.7	13.56	-39.75	-6.123	2.93	0.00	2.93
8.645	21.5	7.16	-44.72	-6.888	1.49	0.00	1.49
9.100	0.0	0.00	-49.69	-7.653	0.00	0.00	0.00