

30.6kN

Title:	Access and vertical	propping to the	max <b>Jo</b>	b No:	1529-1-2-3	3- Rev	
	Car Park, Peterboro	use at The Markough.	et Sh	eet No:	<b>4-5-6-</b> 7 1	Date Of	20
Contractor:			Pr	epd By:	SMC	Date:	23.9.19
			Ch	ıkd By:		Date:	
<u>Materials</u>		Standard scaffol	d tube in acc	cordance wit	h TG20:13,		
		All tube will be ga Fittings in accord	alvanised th Jance with B	nerefore take SS 1139.	e as new.		
<u>Properties of</u>	<u>tube.</u>	Outside diamete Weight Z I r Area Allowable BM. Allowable shear	r	= 48. = 4.3 = 5.7 = 13 = 1.5 = 5.5 = 1.1 = 29.	3 mm 37 kg/m 70 cm3 .8 cm4 57 cm 57 cm2 2kNm 1kN		
<u>Scaffold boar</u>	<u>ds</u>	(225 x 38 mm) Allowable BM. Self weight		= 0.4 = 0.2	8 kNm 25 kN/m2		
<u>Allowable tuk</u>	be strut loads.	<b>Length (mm)</b> 1000 1200 1400 1600	Load (kN) 58.6 51.9 45.3 39.2		Length (mm) 1800 2000 2200 2400	<b>Load</b> 33.7 29.1 25.3 22.0	(kN)
<u>Allowable fitt</u>	<u>ing loads.</u>	<b>Type of fitting</b> Right Angle Right Angle SGB Mk3A Swivel Sleeve Brace DH Putlog Coupler Adj. Base/FH	Ту	<b>rpe of load</b> Slip Slip Slip Tension Slip Slip Axial	s	<b>5.W.L (kN)</b> 6.1 (class A) 9.1 (class B) 12.5 6.1 3.6 5.0 0.63 30.0	
<u>Allowable BN</u>	I. & shear for scaffo	<b>blding beams.</b> <b>Type beam</b> Unit beam Surebeam SGB Soldier Mk Haki 400 Alumir	2 nium Truss	<b>Allowable</b> 27.7kNm ( 13.5kNm 38.0kNm	<b>BM.</b> bolt shear) (10.0kNm at jo 5.7kNm	<b>Allowa</b> 20 18 int) 75 12	<b>ble reaction</b> ).0kN .0kN 5.0kN .7kN

Note - Not all materials listed will be used in the following design

41.3kNm

Haki 750 Aluminium Truss



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These calculations are for the access and vertical propping all as shown on DSD drawings 19-1529-1, 19-1529-2, 19-1529-3, 19-1529-4, 19-1529-5, 19-1529-6 and 19-1529-7. Loads allowed for to the scaffold

#### Vertical loads to propping scaffold =

Self weight of slab = 6.72kN/m<sup>2</sup> Live load on the slab = 1.5kN/m<sup>2</sup> Therefore total vertical load allowed for per floor level = 8.22kN/m<sup>2</sup> all as specified by Rolton Group.

#### No additional vertical or horizontal loads have been accounted for on this scaffold!

#### Live load to the access scaffold

Live load to the access scaffold is allowed for at 2.0kN/m<sup>2</sup> at one level plus second level all at 0.75kN/m<sup>2</sup>. One additional level all at 0.75kN/m<sup>2</sup> is allowed for as protection at first lift.

All loads must be checked to ensure they are adequate and not exceeded and the existing ground / structure must be checked to ensure they can safely support the imposed loads in all areas. All checks to be done by others.

#### Access Leg loads

Scaffold constructed in 2.0m lifts with a 2.7m pavement gantry, in accordance with TG20 the effective length of scaffold uprights = 2.7m therefore the permissible axial loads in uprights = 18.2kN

#### Inside Leg

Inside Standards	kg	Fittings
$1 \times 2.0 m$ standard = $2.0 m$	2.0m x 4.4kg/m = 8.8kg	
1 x 2.0m ledger = 2.0m	2.0m x 4.4kg/m = 8.8kg	1 x 1kg = 1kg
4 x 0.8m transom = 3.2m	3.2m x 4.4kg/m = 14.08kg	4 x 1kg = 4kg
$1 \times 2.0 m$ handrail = $2.0 m$	2.0m x 4.4kg/m = 8.8kg	1 x 1kg = 1kg
1 x 1.3m ledger brace = 1.3m	1.3m x 4.4kg/m = 5.72kg	1 x 1kg = 1kg
Total weight	46.2kg	7kg
Total self weight per node =	46.2 + 7 = 53.2kg =	0.52kN



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Boards =  $0.225 \times 2.5 \times 2.0 \times 0.25$ kN/m<sup>2</sup> = 0.28kN Live =  $0.225 \times 2.5 \times 2.0 \times (2.0$ kN/m<sup>2</sup> + 0.75kN/m<sup>2</sup> + 0.75kN/m<sup>2</sup>) = 3.94kN

Total leg load = 0.52kN x 8 + 0.28kN x 9 + 3.94kN = 10.62kN < 18.2kN permissible therefore OK

#### **Outside Leg**

Outside Standards	kg	Fittings
$1 \times 2.0 m$ standard = $2.0 m$	2.0m x 4.4kg/m = 8.8kg	
1 x 2.0m ledger = 2.0m	2.0m x 4.4kg/m = 8.8kg	1 x 1kg = 1kg
4 x 0.8m transom = 3.2m	3.2m x 4.4kg/m = 14.08kg	4 x 1kg = 4kg
1 x 1.3m ledger brace = 1.3m	1.3m x 4.4kg/m = 5.72kg	1 x 1kg = 1kg
$2 \times 2.0 \text{m}$ handrail = $4.0 \text{m}$	4.0m x 4.4kg/m = 17.6kg	2 x 1kg = 2kg
1 x 1.5m face brace = 1.5m	1.5m x 4.4kg/m = 6.6kg	1 x 1kg = 1kg
Total weight	61.6kg	9kg
Total weight per node =	61.6 + 9 = 70.6kg =	0.69kN

Boards =  $0.225 \times 3.5 \times 2.0 \times 0.25$ kN/m<sup>2</sup> = 0.393kN Live =  $0.225 \times 2.5 \times 2.0 \times (2.0$ kN/m<sup>2</sup> + 0.75kN/m<sup>2</sup> + 0.75kN/m<sup>2</sup>) = 3.94kN Total leg load = 0.69kN x 8 + 0.393kN x 9 + 3.94kN = 12.99kN < 18.2kN permissible therefore OK

Tie loads from external access

#### Wind loads from BS EN 1991-1-4

Fundamental basic wind speed =  $V_f = V_m \times C_{alt}$ 

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 $V_m = From figure NA.1 = 22$ Altitude from Google Earth at 14m  $C_{alt} = 1 + 14 \div 1000$  $C_{alt} = 1.014$  $V_m = 22 \times 1.014$  $V_f = 22.308$ 

 $\begin{array}{l} \text{Basic wind speed} = \\ V_b = V_f \ x \ C_{\text{dir}} \ x \ C_{\text{season}} \ x \ C_{\text{prob}} \\ V_b = 22.308 \ x \ 1 \ x \ 1 \ x \ 1 \\ V_b = 22.308 \end{array}$ 

 $\begin{array}{l} \text{Basic wind pressure} = \\ q_{b} = 0.613 \ x \ V_{b}{}^{2} \div 1000 \\ q_{b} = 0.613 \ x \ 22.308^{2} \div 1000 \\ q_{b} = 0.305 \end{array}$ 

Peak wind pressure =  $q_p = q_b \times C_e$   $q_b = 0.305$   $C_e = Figure NA.7$  at max 18m high at 40km to shoreline = 2.8  $C_{eT} = Figure NA.8$  at max 18m high 0.1km in town = 1.0  $q_p = 0.305 \times 2.8 \times 1$  $q_p = 0.854$ 

 $C_sC_d$  taken as 1.0 Therefore wind = 0.854 x 1.0 = 0.854kN/m<sup>2</sup>

Temporary structure factor taken from EN 12811 = 0.7 therefore wind = 0.854 x 0.7 = 0.598kN/m<sup>2</sup>

Car park considered with wind as for fully clad building due to full sheeting to perimeter (all sides to be clad at all times)

 $C_{pe}$  taken from BS EN 1991-1-4 table 7.1. Wind considered to zone A, D & B

 $\begin{array}{l} C_{\rm pe} \; \text{zone} \; A = -1.2 \; x \; 0.598 k N/m^2 = -0.7176 k N/m^2 \\ C_{\rm pe} \; \text{zone} \; D = 0.8 \; x \; 0.598 k N/m^2 = 0.478 k N/m^2 \\ C_{\rm pe} \; \text{zone} \; B = -0.8 \; x \; 0.598 k N/m^2 = -0.478 k N/m^2 \end{array}$ 



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Scaffold to be tied to the existing structure with shear anchors to the underside of the slab or by box ties to the existing columns to every floor at every frame in zone A and at every other frame at Zone B therefore maximum area per tie =

Zone A = 2.0m x 2.55m vertical =  $5.1m^2$ Zone B = 4.0m x 2.55m vertical =  $10.2m^2$ 

Tie loads Zone A =  $5.1m^2 \times -0.7176kN/m^2 = 3.66kN$ Zone B =  $10.2m^2 \times -0.478kN/m^2 = 4.87kN$ 

Increased tie area to top tie per frame =  $2.0m \times 4.1m$  vertical =  $8.2m^2$ Fix ties to top lift at every frame therefore; Zone A maximum tie load =  $8.2m^2 \times -0.7176$ kN/m<sup>2</sup> = 5.88kN Zone B maximum tie load =  $8.2m^2 \times -0.478$ kN/m<sup>2</sup> = 3.92kN Positive loads to zone D =  $8.2m^2 \times -0.478$ kN/m<sup>2</sup> = 3.92kN max in all areas

Note – during the demolition process each level becomes the top tied lift and therefore all ties to be taken top tie level case

Check moment though two hole band for pull out load, anchor fixed in one hole only, furthest away from external scaffold as shown on drawing.





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Zone A (negative loads) = Moment = 5.88kN x 0.075m = 0.441kNm Force = 0.441kNm  $\div 0.097$ m = **4.54kN** 

Zone B (negative loads) = Moment = 3.92kN x 0.075m = 0.294kNm Force = 0.294kNm  $\div 0.097$ m = 3.03kN

Zone D (positive loads) = Moment = 3.92kN x 0.075m = 0.294kNm Force = 0.294kNm  $\div 0.033$ m = **8.91kN** 

Resulting worst case loads to anchor = Zone A with 5.88kN shear and 4.54kN tension Zone D with 3.92kN shear and 8.91kN tension

Anchors to be fixed as 130mm long 12mm ADI self-tapping concrete bolt through the back of a band and plate as shear tie each with permissible shear of 15kN per bolt and permissible tension load of 13kN

#### Check COMBINED anchor bolt loading:

Zone A = Combined loading =  $\frac{fs}{Fs}$  +  $\frac{ft}{Ft}$  < 1.2 as TG4:11 =  $\frac{5.88}{15}$  +  $\frac{4.54}{13}$  = 0.74 (< 1.2) OK Zone D = Combined loading =  $\frac{fs}{Fs}$  +  $\frac{ft}{Ft}$  < 1.2 as TG4:11

= <u>3.92</u> + <u>8.91</u> = 0.946 (< 1.2) <u>OK</u> 15 13

Ties to be tested in accordance with TG4 at 1.25 x required load therefore increased proof test required =  $8.91 \times 1.25 = 11.14$ kN



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#### Vertical propping

Total load allowed for per floor level = 8.22kN/m<sup>2</sup> all as specified by Rolton Group

All propping to be constructed in a maximum grid size of 2.0m x 2.0m with props at each level positioned directly above props below. Therefor maximum load per prop line per floor =  $2.0m \times 2.0m \times 8.22 \text{kN/m}^2$  = 32.88 kN

Self weight of the propping system at each level =

<u>Tubular props on 5<sup>th</sup> floor =</u> Uprights = 2.0m x 2 = 4m Ledgers / transoms = 2.0m x 4 = 8m Ledger bracing / face bracing =  $1.5m \times 2 = 3m$ 

Total =  $(4m + 8m + 3m) \times 4.4$ kg/m + 8 fittings x 1kg = 74kg 74kg x 9.81 ÷ 1000 = 0.725kN

Soleboards = 0.225m x 0.7m x 4 x 0.25kN/m<sup>2</sup> = 0.15kN

Total self weight = 0.15kN + 0.725kN = 0.88kN

<u>Single soldier props on  $4^{th}$  floor =</u> Threaded shoring adaptor = 12.7kg Tubular shoring adaptor = 5.2kg 1.125m soldier = 25.43kg Ledgers / transoms = 2.0m x 4 = 8m Ledger bracing / face bracing = 1.5m x 2 = 3m

Total = (8m + 3m) x 4.4kg/m + 8 fittings x 1kg + 25.43kg + 5.2kg + 12.7kg = 99.73kg 99.73kg x 9.81 ÷ 1000 = 0.978kN

Soleboards =  $0.225m \times 0.7m \times 4 \times 0.25kN/m^2 = 0.15kN$ 

Total self weight = 0.15kN + 0.978kN = 1.13kN

<u>Single soldier prop with single tubular prop on 3<sup>rd</sup> floor =</u> Threaded shoring adaptor = 12.7kg Tubular shoring adaptor = 5.2kg 1.125m soldier = 25.43kg Upright = 2.0m



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Ledgers / transoms = 2.0m x 4 = 8m Ledger bracing / face bracing = 1.5m x 2 = 3m

Total = (2.0m +8m + 3m) x 4.4kg/m + 10 fittings x 1kg + 25.43kg + 5.2kg + 12.7kg = 110.53kg 110.53kg x 9.81 ÷ 1000 = 1.08kN

Soleboards =  $0.225m \times 0.7m \times 4 \times 0.25kN/m^2 \times 2 = 0.3kN$ 

Total self weight = 0.3kN + 1.08kN = 1.38kN

<u>Double soldier props on  $2^{nd}$  and  $1^{st}$  floors =</u> Threaded shoring adaptor = 12.7kg x 2 = 25.4kg Tubular shoring adaptor = 5.2kg x 2 = 10.4kg 1.125m soldier = 25.43kg x 2 = 50.86kg Ledgers / transoms = 2.0m x 4 = 8m Ledger bracing / face bracing = 1.5m x 2 = 3m

Total = (8m + 3m) x 4.4kg/m + 12 fittings x 1kg + 50.86kg + 10.4kg + 25.4kg = 147.06kg 147.06kg x 9.81 ÷ 1000 = 1.44kN

Soleboards =  $0.225m \times 0.7m \times 4 \times 0.25kN/m^2 \times 2 = 0.3kN$ 

Total self weight = 0.3kN + 1.44kN = 1.74kN

<u>Double soldier props with tubular prop on ground floor =</u> Threaded shoring adaptor = 12.7kg x 2 = 25.4kg Tubular shoring adaptor = 5.2kg x 2 = 10.4kg 1.8m soldier = 37.42kg x 2 = 74.84kg Upright = 2.0m Ledgers / transoms = 2.0m x 4 = 8m Ledger bracing / face bracing = 1.5m x 2 = 3m

Total = (2m + 8m + 3m) x 4.4kg/m + 14 fittings x 1kg + 74.84kg + 10.4kg + 25.4kg = 181.84kg 181.84kg x 9.81 ÷ 1000 = 1.78kN

Soleboards = 0.225m x 0.7m x 4 x 0.25kN/m<sup>2</sup> x 2 = 0.3kN

Total self weight = 0.3kN + 1.78kN = 2.08kN



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Therefore loads per level from structure and self weight of propping system = Tubular scaffold props constructed on floor level 5 load = 32.88kN + 0.88kN = 33.76kN Single soldier prop constructed on floor level 4 load = 33.76kN + 32.88kN = 66.64kN Single soldier prop with tubular prop constructed on floor level 3 load = 66.64kN + 32.88kN = 98.64kN Double soldier props constructed on floor level 2 load = 32.88kN x 4 = 131.52kN Double soldier props constructed on floor level 1 load = 32.88kN x 5 = 164.44kN Double soldier props with tubular prop constructed on floor level 1 load = 32.88kN x 5 = 164.44kN

Floor level	Cumulative loads from existing structure and props from floors above	Total load at floor level immediately above prop level	Self weight propping	Total load at floor level
6 <sup>th</sup> Floor	-	-	-	
5 <sup>th</sup> Floor	-	32.88kN	0.88kN	33.76kN
4 <sup>th</sup> Floor	33.76kN	32.88kN	1.13kN	67.77kN
3 <sup>rd</sup> Floor	67.77kN	32.88kN	1.38kN	102.03kN
2 <sup>nd</sup> Floor	102.03kN	32.88kN	1.74kN	136.65kN
1 <sup>st</sup> Floor	136.65kN	32.88kN	1.74kN	171.27kN
Ground	171.27kN	32.88kN	2.08kN	206.23kN

The existing structure must be checked to ensure that it is capable of safely transmitting the loads from one level to another and the existing ground level must be checked to ensure it is capable of safely supporting the loads specified, all by others. Some existing partition walls, toilets and toilet cubicles will need to be removed prior to the start of construction. All making good necessary of ground floor around toilet waste pipes etc to be designed supplied and fixed by other and must be capable of supporting the loads specified.



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#### Props fixed per level

#### 5<sup>th</sup> Floor

Prop load = 33.76kN

Props to be fixed as pairs of tubular uprights each fixed with adjustable base plates with a minimum safe working load of 30kN.

The scaffold is to be fully braced with 1.8m maximum lift heights, in accordance with TG20 the effective length of the uprights including a k factor of  $1.1 = 1.8m \times 1.1 = 1.98m$  taken as 2.0m resulting in a permissible axial load of 29.1kN.

Therefore capacity of props = 29.1kN x 2 = 58.2kN > 33.79kN therefore OK

#### 4<sup>th</sup> Floor

Prop load = 67.77kN Props to be fixed as single lines of soldier props with a minimum safe working load of 100kN > 67.77kN therefore OK

#### 3<sup>rd</sup> Floor

Prop load = 102.03kN Props to be fixed as single lines of soldier props with an adjacent tubular prop.

Tubular props to be fixed with adjustable base plate with a minimum safe working load of 30kN. The scaffold is to be fully braced with 1.0m maximum lift heights, in accordance with TG20 the effective length of the uprights including a k factor of  $1.1 = 1.0m \times 1.1 = 1.1m$  resulting in a permissible axial load of 51.9kN. The top un braced lift of the tubular uprights is taken with an effective length of I x 2 = 0.8m x 2 = 1.6m resulting in a permissible axial load of 39.2kN. Therefore item limiting capacity of tubular upright is adjustable base at 30kN

Soldier props to be fixed as single lines of soldier props with a minimum safe working load of 100kN

Therefore capacity of props = 100kN + 30kN = 130kN > 102.03kN therefore OK



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#### 2<sup>nd</sup> Floor

Prop load = 136.65kN Props to be fixed as double lines of soldier props each with a minimum safe working load of 100kN therefore capacity of props = 100kN x 2 = 200kN > 136.65kN therefore OK

#### 1<sup>st</sup> Floor

Prop load = 171.27kN Props to be fixed as double lines of soldier props each with a minimum safe working load of 100kN therefore capacity of props = 100kN x 2 = 200kN > 171.27kN therefore OK

#### **Ground Floor**

Prop load = 206.23kN Props to be fixed as double lines of soldier props with an adjacent tubular prop.

Tubular props to be fixed with adjustable base plate with a minimum safe working load of 30kN. The scaffold is to be fully braced with 1.6m maximum lift heights, in accordance with TG20 the effective length of the uprights including a k factor of  $1.1 = 1.6m \times 1.1 = 1.76m$  taken as 1.8m resulting in a permissible axial load of 33.7kN. The top un braced lift of the tubular uprights is taken with an effective length of I x 2 = 0.8m x 2 = 1.6m resulting in a permissible axial load of 39.2kN. Therefore item limiting capacity of tubular upright is adjustable base at 30kN

Soldier props to be fixed as double lines of soldier props with a minimum safe working load of 100kN x 2 = 200kN

Therefore capacity of props = 200kN + 30kN = 230kN > 206.23kN therefore OK



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#### Props to car park ramps

Props to car park ramps to be fixed with swivel shoring base with 90kN capacity.

Therefore props fixed per level

#### 5<sup>th</sup> Floor

Prop load = 33.76kN Props to be fixed as single lines of soldier props with a minimum safe working load of 90kN > 33.76kN therefore OK

#### 4<sup>th</sup> Floor

Prop load = 67.77kN Props to be fixed as single lines of soldier props with a minimum safe working load of 90kN > 67.77kN therefore OK

#### 3<sup>rd</sup> Floor

Prop load = 102.03kN Props to be fixed as double lines of soldier props each with a minimum safe working load of 90kN therefore capacity of props = 90kN x 2 = 180kN > 102.03kN therefore OK

#### 2<sup>nd</sup> Floor

Prop load = 136.65kN Props to be fixed as double lines of soldier props each with a minimum safe working load of 90kN therefore capacity of props = 90kN x 2 = 180kN > 136.65kN therefore OK



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#### 1<sup>st</sup> Floor

Prop load = 171.27kN

Props to be fixed as double lines of soldier props each with a minimum safe working load of 100kN therefore capacity of props =  $90kN \times 2 = 180kN > 171.27kN$  therefore OK

#### **Ground Floor**

Prop load = 206.23kN

Props to be fixed as triple cluster of soldier props each with a minimum safe working load of 90kN therefore capacity of props =  $90kN \times 3 = 270kN > 206.23kN$  therefore OK



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Refer to page 35 (Tubular Adaptor) or page 36 (Threaded Adaptor). 7) For minor axes of Soldiers lace tubes are fixed using the Soldier Bracing Couplers. For major axes of Soldiers lace tubes are fixed to minor axis lacing using Double Couplers. Brace tubes may be fixed to lace tubes with Swivel Couplers (lace & brace parallel) or to lace tubes with Double Couplers (lace & brace at right angles). S.W.L SGB Double & Swivel Couplers 6.25 kN, SGB Mk3A Double Coupler 12.5 kN



Title:	Access and vertical propping to the max loads specified for use at The Market Car Park, Peterborough.	Job No: Sheet No:	<b>1529-1-2-3-</b> <b>4-5-6-7</b> 16	Rev Date <b>Of</b>	20
Contractor:		Prepd By:	SMC	Date:	23.9.19
		Chkd By:		Date:	





Title:	Access and vertical propping to the max loads specified for use at The Market Car Park, Peterborough.	Job No: Sheet No:	1529-1-2-3- 4-5-6-7 17	Rev Date <b>Of</b>	20
Contractor:		Prepd By:	SMC	Date:	23.9.19
		Chkd By:		Date:	





Title:	Access and vertical propping to the max loads specified for use at The Market Car Park, Peterborough.	Job No: Sheet No:	<b>1529-1-2-3-</b> <b>4-5-6-7</b> 18	Rev Date <b>Of</b>	20
Contractor:		Prepd By:	SMC	Date:	23.9.19
		Chkd By:		Date:	



**Contractor:** 



Title: Access and vertical propping to the max loads specified for use at The Market Car Park, Peterborough.

1529-1-2-3-	Rev	
4-5-6-7	Date	
19	Of	20
SMC	Date:	23.9.19
	Date:	
	<b>1529-1-2-3-</b> <b>4-5-6-7</b> 19 SMC	1529-1-2-3- Rev   4-5-6-7 Date   19 Of   SMC Date:   Date: Date:

N/A 220

140

120 170

120

100

80

N/A N/A

Data applies to hex and hex flange head styles only

Loads in C20/25 Concrete

All dimensions in mm unless otherwise shown

Normal Spacing Distance (Tensile)

Normal Edge Distance (Shear)

90

200

West Midlands. DY5 3LB Tel: 01384 483657 ADI Supply Ltd Units 16-17 Meeting Lane Industrial Estate, Off Station Drive, Brierley Hill Fax: 01384 483663 sales@adisupply.co.uk www.adisupply.co.uk

> SBS **Technical Data Sheet** Product Designation

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**Finish** : Zinc & Yellow Passivated (thickness 3~5 Microns CS Bolts are a single fixing solution for the majority of construction materials which are very easy to install and have high pull out and shear values. They can also be used close to an edge without breaking the substrate. Suitable for brick, wood, marble, block & stone. Self Tapping Concrete/ Masonry Bolt Hardened Steel Material Type

007×91 200 70 120 120 155 N/A N/A 18 2 150 0ST×9T 100 100 27 18 001×91 100 20 115 N/A N/A 80 40 200 140 007×71 150 90 OSIXZI 6 115 60 13 22 12 70 130 081×21 8 80 19 14 100 15×100 15 40 13.5 09 85 26 54 6.5 52×21 75 150 OSTXOT 100 061×01 130 80 12.5 75 95 50 36 6 10 20 12 80 00T×0T 8 17 SZXOT 75 25 4.5 50 70 18 40 10 09×0T 60 10 150 110 05TX8 130 90 08X130 8 75 30 30 7.5 9 100 001×8 60 9 15 10 60 20 35 57x8 75 40 55 12 24 9 60 09×8 150 105 OSTX9 85 130 02130 45 55 3.5 16 14 4 100 N/A 60 22 10 00T×9 5 75 5**ZX9** 45 2.5 30 40 10 2 20 05×9 20 001×5 100 63 37 47 9.6 Ħ 4.8 5.5 75 20 SZXS N/A N/A 15 25 50 05×5 52 4.2 2.1 4.5 35 6 s 08×3 30 Maximum Allowable Tensile Action (kN) Maximum Allowable Shear Action (kN) Mean Ultimate Tensile Action (kN) Mean Ultimate Shear Action (kN) Normal Edge Distance (Tensile) Maximum Fixing Thickness Installation Torque (Nm) Minimum Embedment Minimum Hole Depth Washer Diameter Anchor Length **Drill Diameter** A/F Size Setting Details hmin tinst Num Vum Nrec tfix Vrec AF HZ 吕 4

CONSTRUCTION F | XINGS APPROVED C

CSB12 Masonry Screw Bolt 1<sup>4</sup> August 2014 Rev 2.0 Page 1 of 2



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Registered in the UK 05002500







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Title:	Access and vertical propping to the max loads specified for use at The Market	Job No:	1529-1-2-3- 4-5-6-7	Rev Date	
	Car Park, Peterborough.	Sheet No:	20	Of	20
Contractor:		Prepd By:	SMC	Date:	23.9.19
		Chkd By:		Date:	

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Tensile Tensile 10

Tensile

12

200

170

90 0.93 0.92 0.71

80 0.86 0.89 0.70

20 0.80 0.87 0.70

60 0.73 0.84 0.69

0.66 50 0.81

40 0.59 0.78

Size mm Edge mm 20 30 6 Tensile 0.52 Spacing Reduction Factors

III II II III

00

0.84 1.00 0.85 0.92

0.73 1.0

0.95

Edge Reduction Factors

- nAn-	audion 1	auto	2							Contraction of the local distance of the loc				
Size mm	Edge mm	20	30	40	50	09	70	80	06	100	110	120	130	140
9	Tensile	0.70	0.80	0.86	0.95	1.00								
8	Tensile	0.61	0.72	0.84	0.93	1.00								
10	Tensile		0.43	0.63	0.80	0.92	1.00							
12	Tensile			0.57	0.62	0.70	0.77	0.85	0.90	1.00				
9	Shear	0.35	0.52	0.70	0.78	0.85	0.92	1.00						
80	Shear			0.32	0.40	0.48	0.65	0.83	1.00					
10	Shear					0.33	0.39	0.51	0.63	0.76	0.88	1.00		
12	Shear							0.32	0.36	0.48	0.61	0.74	0.87	1.00

Edge & spacing reduction factors are based on minimum embedments only In Concrete C20/25 Data for 5mm & 16mm are currently not available